

THERMOCHIP HOUSING

THERMOCHIP

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www.thermochip.com



warm, temperate climate



**CERTIFIED
COMPONENT**

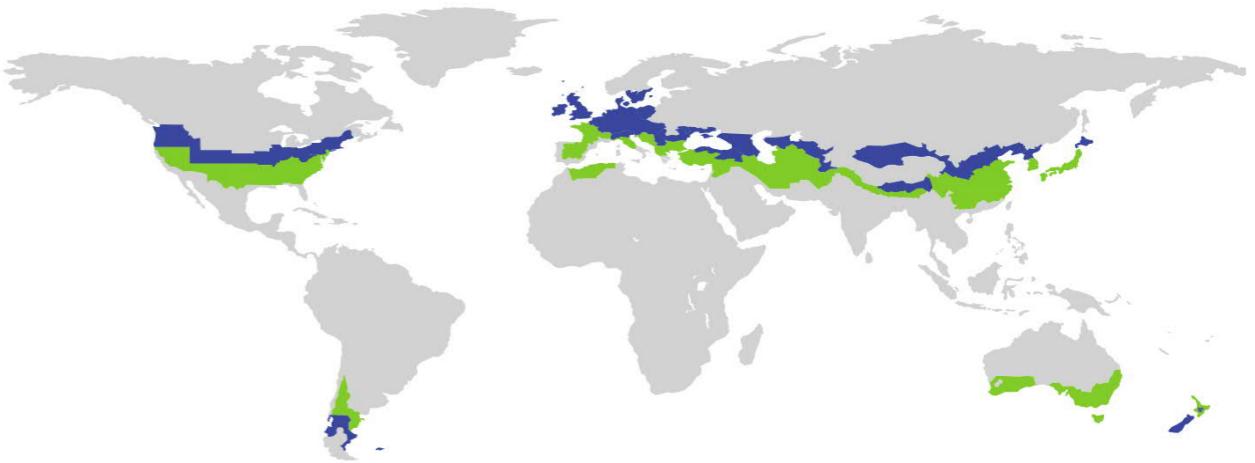
Passive House Institute

CERTIFICATE

Certified Passive House Component

ID: 1625cs04 valid until 31. December 2021

Passive House Institute
Dr. Wolfgang Feist
64342 Darmstadt
GERMANY



Category	Construction system Lightweight timber construction
Manufacturer	Thermochip SLU Carballeda de Valdeorras (Ourense) España
Product name	Thermochip HOUSING SATE-COAT

This certificate for the warm, temperate climate zone was awarded based on the following criteria

Hygiene criterion

The minimum temperature factor of the interior surfaces is

$f_{Rsi=0,25m^2K/W} \geq 0.65$

Comfort criterion

The U-value of the installed windows is

$U_{w,i} \leq 1.05 \text{ W}/(\text{m}^2\text{K})$

Efficiency criteria

Heat transfer coefficient of building envelope

$U^*f_{PHI} \leq 0.30 \text{ W}/(\text{m}^2\text{K})$

Temperature factor of opaque junctions

$f_{Rsi=0,25m^2K/W} \geq 0.82$

Thermal bridge-free design for key connection details

$\Psi \leq 0.01 \text{ W}/(\text{mK})$

An airtightness concept for all components and connection details was provided



Opaque building envelope

With the Thermochip HOUSING Construction System the wintertime thermal insulation of buildings can be ensured. The system is constructed out of timber studs, beams and an outer sandwich panel. The sandwich panel (12/140/12 mm) comprises a board of fibre cement to the outside, a core of XPS ($\lambda=0.036$ W/mK) and internal composite board with cellulose fibres. To the interior a service cavity provides a space for the building services and protects the airtightness layer.

The certification does not take into account point thermal bridges caused by structural columns or e.g. balcony connections, which must be assessed separately. As investigated, the system is deemed suitable for passive houses in the warm-temperate climate zone, as the regular U-values of the exterior components are below 0,25 W/m²K and the connections meet the criteria of 'thermal bridge free'. The surface temperature of all connections (with the exception of window connections) meet the hygiene requirements.

Explanatory notes

The Passive House Institute has defined international component criteria for seven climate zones based on hygiene, comfort and affordability criteria. In principle, components which have been certified for climate zones with higher requirements may also be used in climates with less stringent requirements. Their use might make economic sense in certain circumstances.

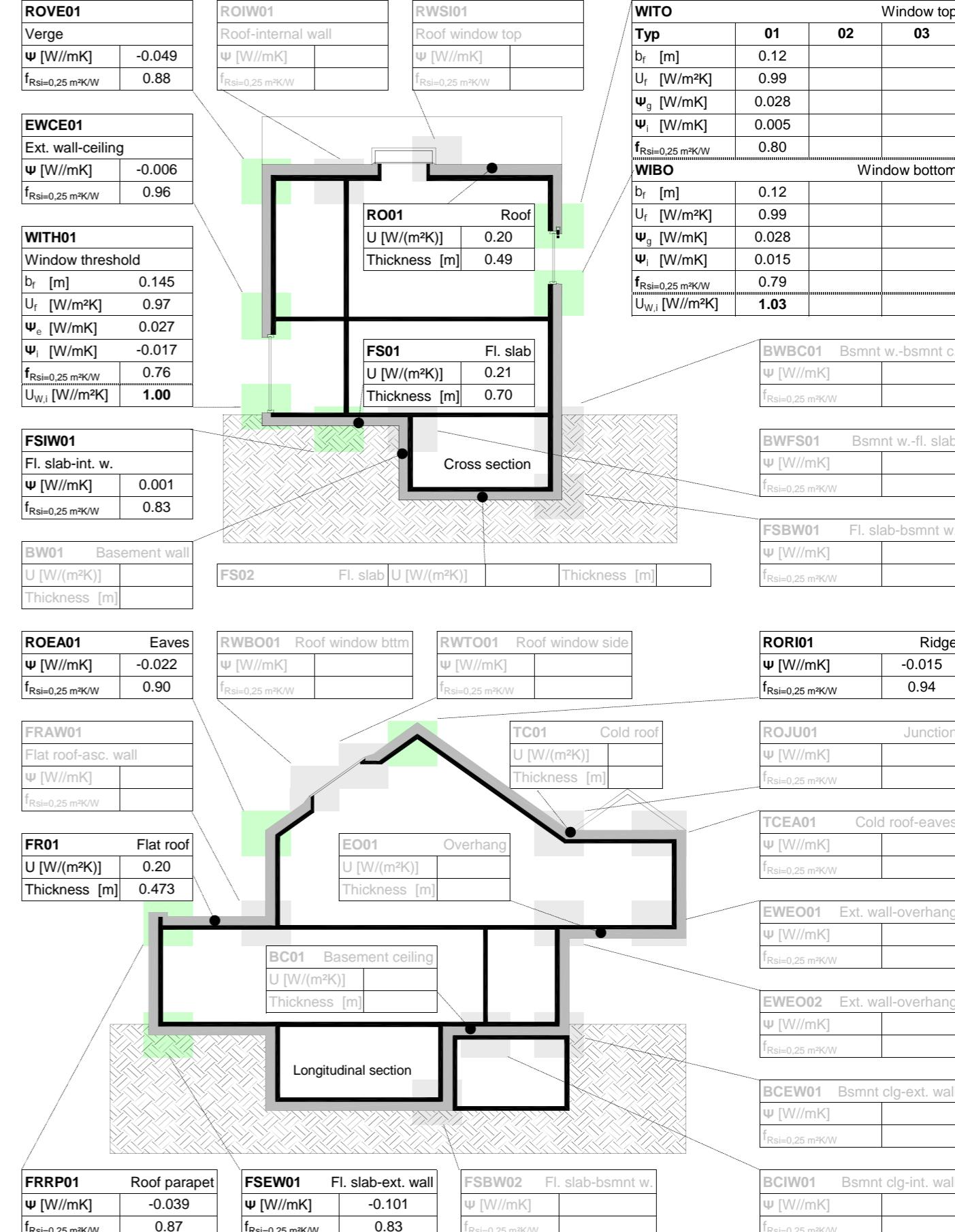
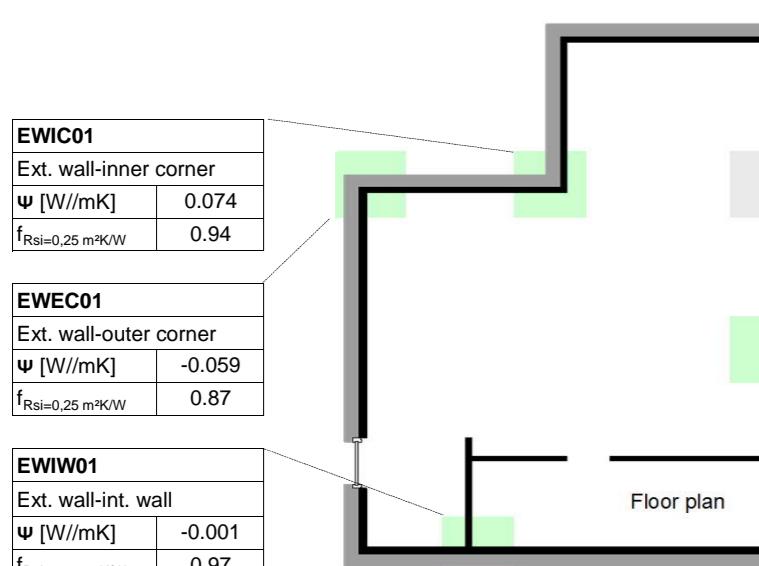
Thermal bridge not calculated
Criteria achieved

Windows

For the purposes of certification a standard passive house window ($U_w = 1,00$ W/m²K with $U_g = 0,90$ W/m²K) was used. The overall U-value of the installed window of standard size (1,23 m wide by 1,48 m tall) should be no more than 0,05 W/m²K greater than the U_w to ensure occupant comfort - this criteria is met in this instance.

Airtightness concept

Airtightness of the system is achieved in the following way: windows and doors are installed with permanently elastic sealing materials and suitable airtight connection membranes and profiles. The airtight layer is located in the gypsum fibre board in the inner side of the sandwich panel. Joints between panels and connections with other building elements are sealed with Soudal Soudatight SP airtight paint.

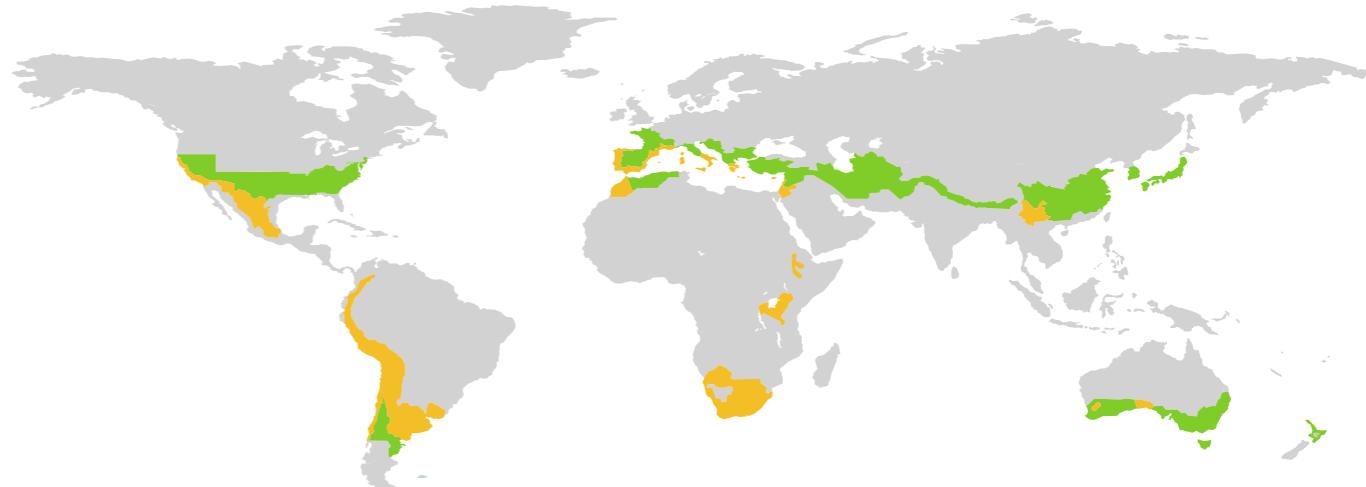


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Temperature factor of opaque junctions

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$\Psi \leq 0.01 \text{ W}/(\text{mK})$

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The certification does not take into account point thermal bridges caused by structural columns or e.g. balcony connections, which must to be assessed separately. As investigated, the system is deemed suitable for passive houses in the warm-temperate climate zone, as the regular U-values of the exterior components are below 0,25 W/m²K and the connections meet the criteria of 'thermal bridge free'. The surface temperature of all connections meet the hygiene requirements.

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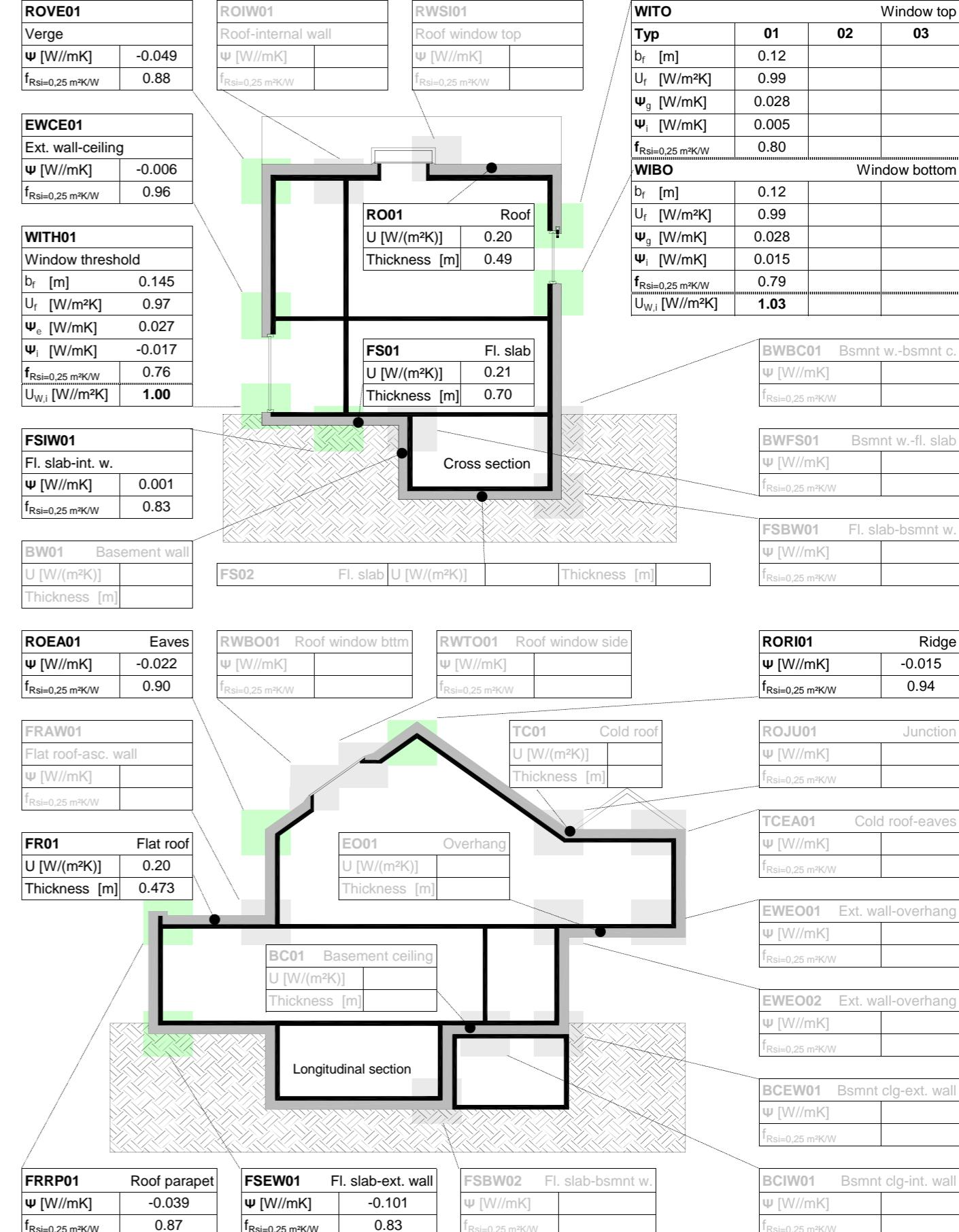
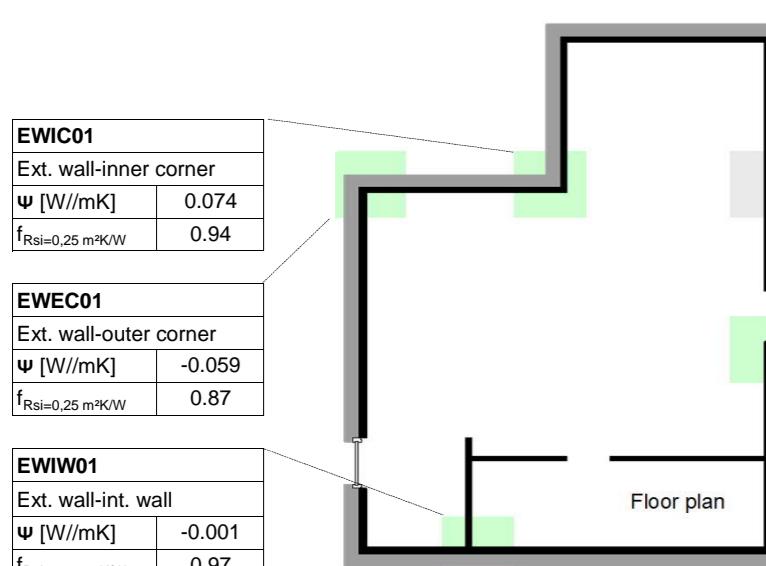
Thermal bridge not calculated
Criteria achieved

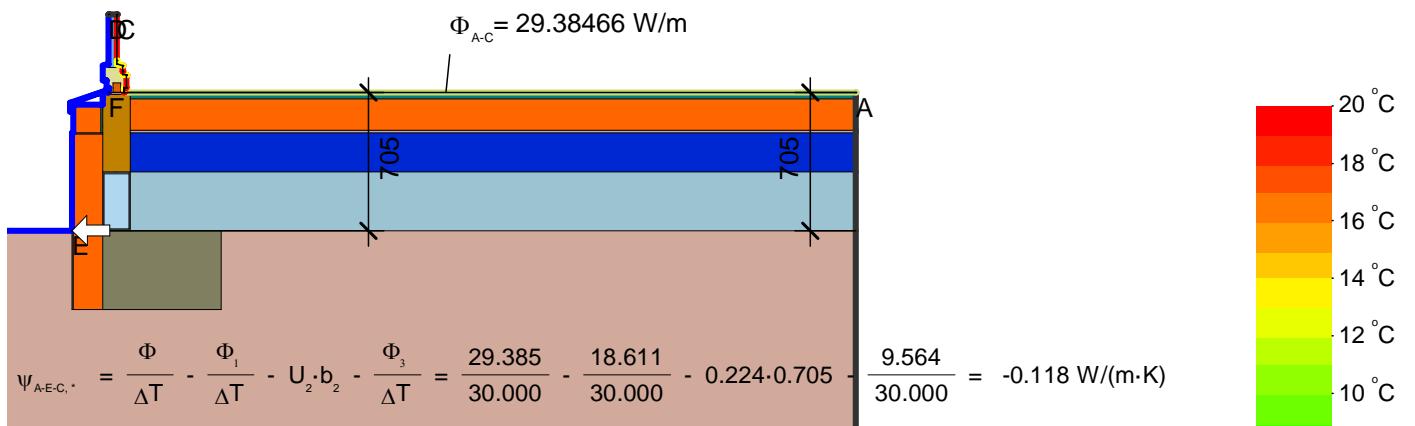
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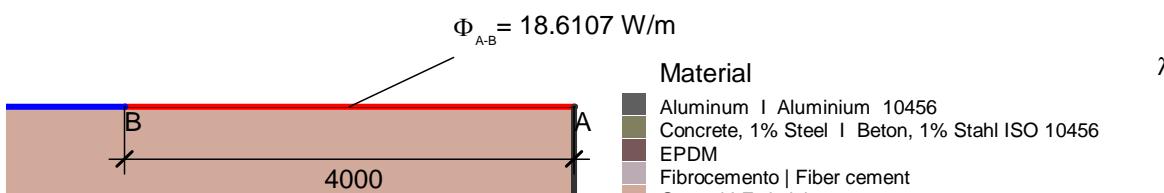
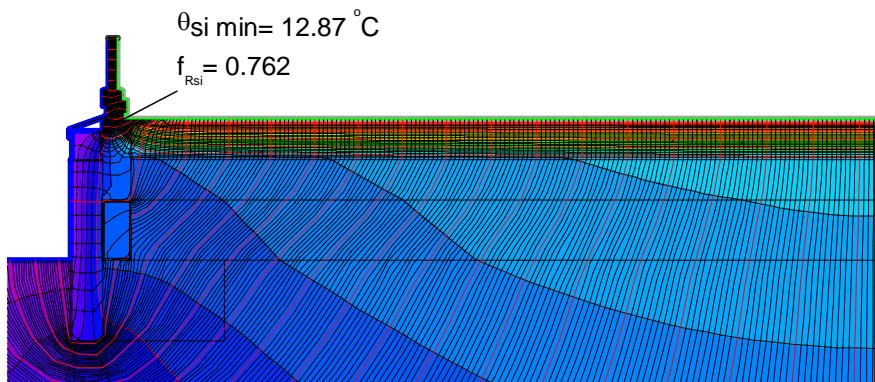
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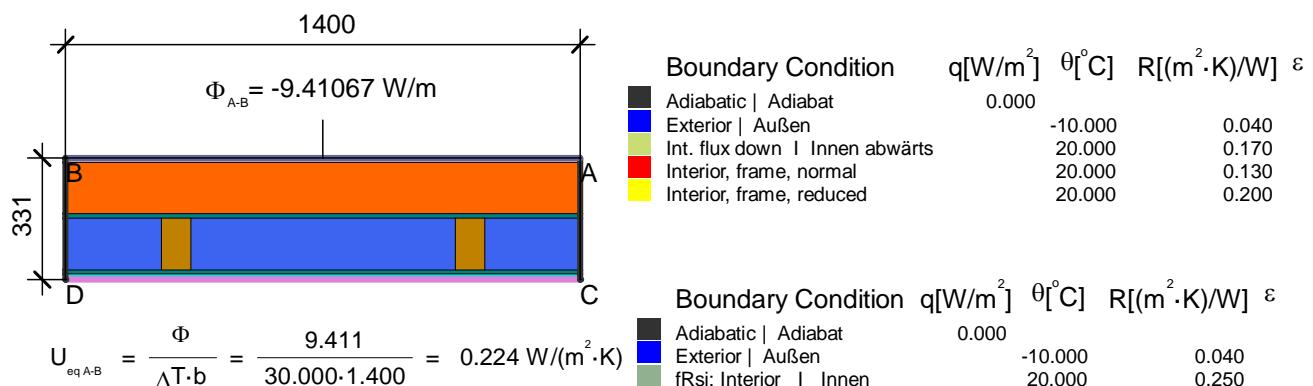
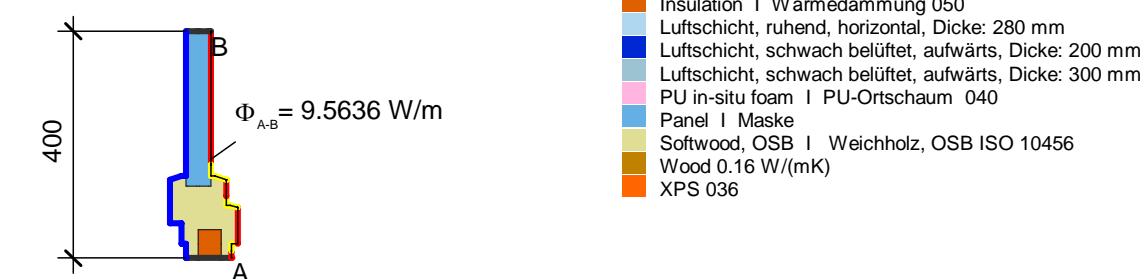


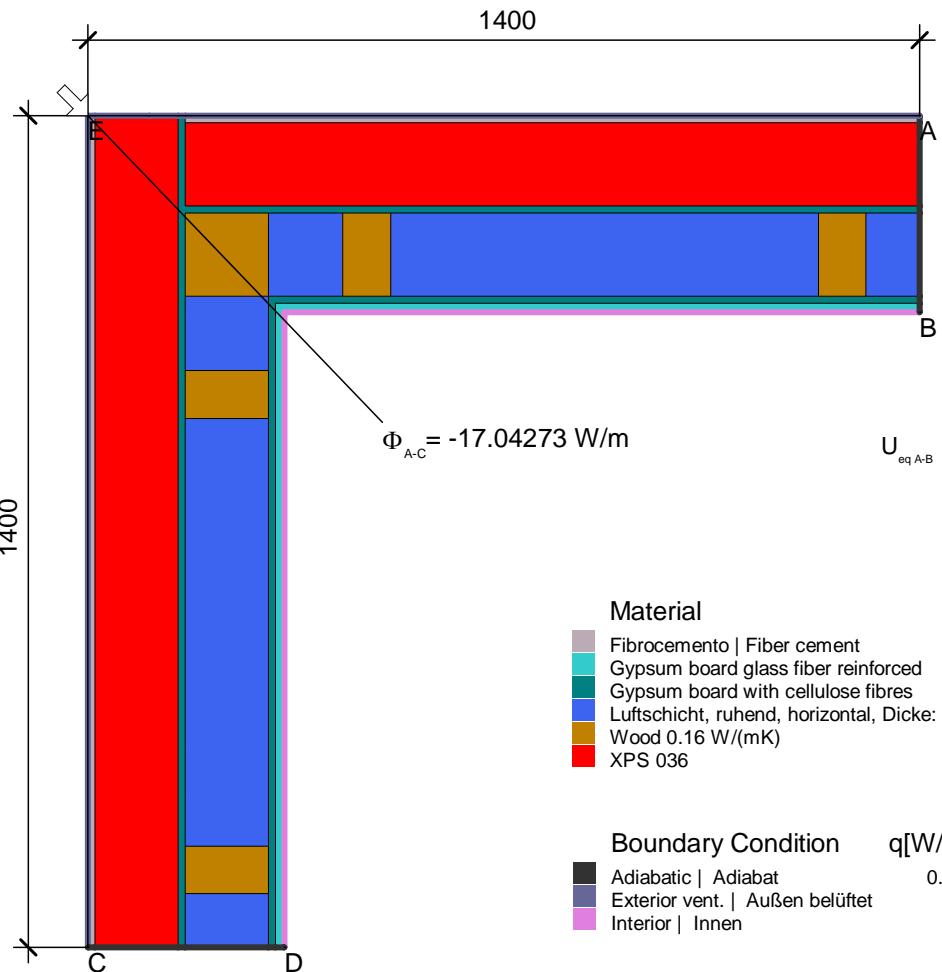


$$\Psi_{WITH} = \Psi_{FSEW+WITH} - \Psi_{FSEW01} = -0.118 - (-0.101) = -0.017 \text{ W/mK}$$

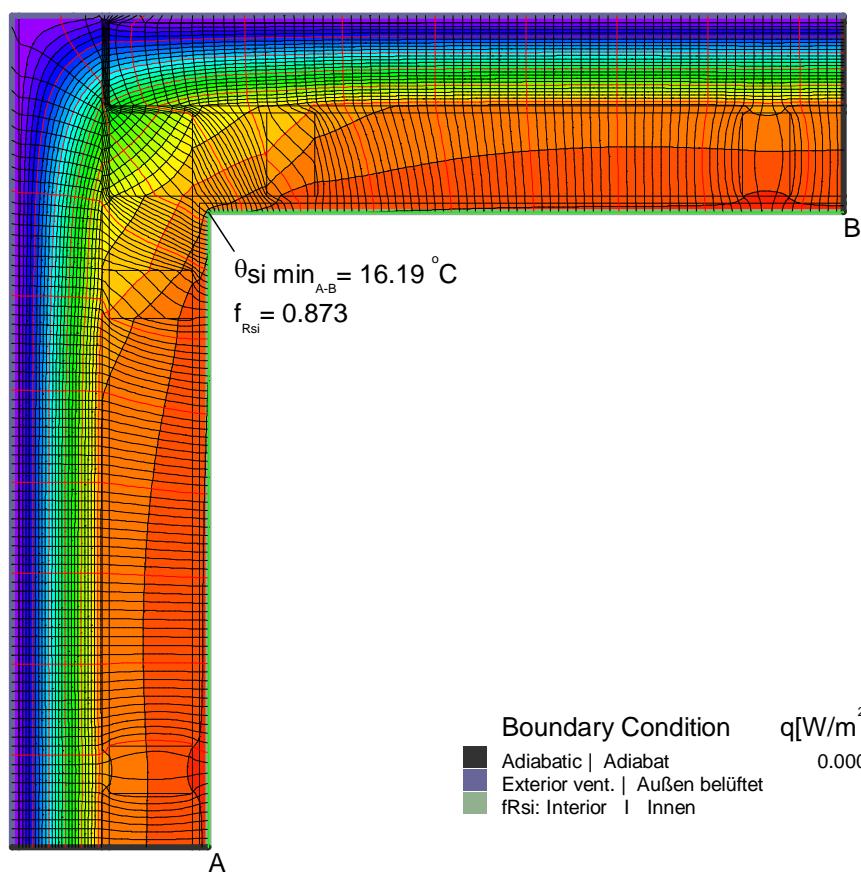


Material	$\lambda [\text{W}/(\text{m}\cdot\text{K})]$	ε
Aluminum Aluminium 10456	160.000	0.900
Concrete, 1% Steel Beton, 1% Stahl ISO 10456	2.300	0.900
EPDM	0.250	0.900
Fibrocemento Fiber cement	1.200	0.900
Ground Erdreich	2.000	0.900
Gypsum board with cellulose fibres	0.669	0.900
Insulation Wärmédämmung 050	0.050	0.900
Luftschicht, ruhend, horizontal, Dicke: 280 mm	1.556	0.900
Luftschicht, schwach belüftet, aufwärts, Dicke: 200 mm	2.500	0.900
Luftschicht, schwach belüftet, aufwärts, Dicke: 300 mm	3.750	0.900
PU in-situ foam PU-Ortschaum 040	0.040	0.900
Panel Maske	0.035	0.900
Softwood, OSB Weichholz, OSB ISO 10456	0.130	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900



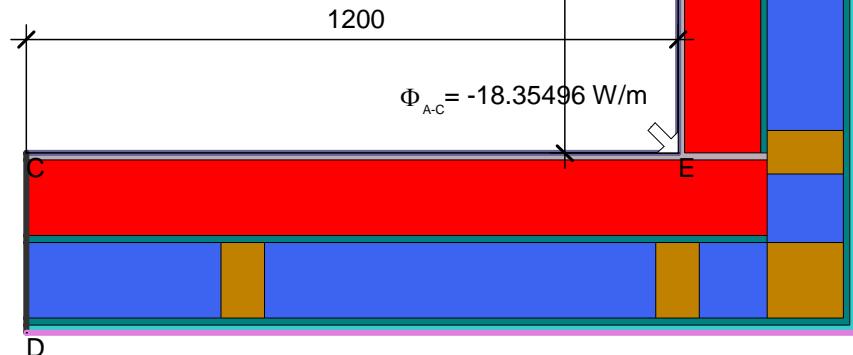


$$\psi_{A-E-C, \cdot} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{17.043}{30.000} - 0.224 \cdot 1.400 - 0.224 \cdot 1.400 = -0.059 \text{ W/(m}\cdot\text{K)}$$

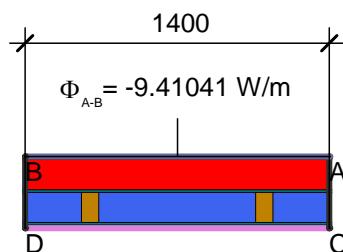


Material	$\lambda[W/(m \cdot K)]$	ε
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Luftschicht, ruhend, horizontal, Dicke: 140 mm (1)	0.778	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

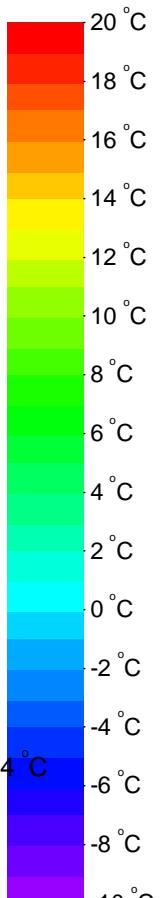
Boundary Condition	$q[W/m^2]$	$\theta[^\circ C]$	$R[(m^2 \cdot K)/W]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet		-10.000	0.130	
Interior Innen		20.000	0.130	



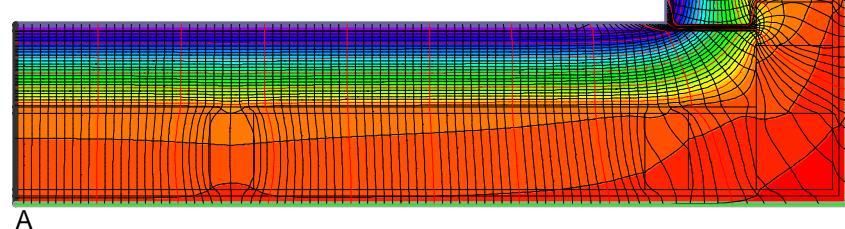
$$\psi_{A-E;C,+} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{18.355}{30.000} - 0.224 \cdot 1.200 - 0.224 \cdot 1.200 = 0.074 \text{ W/(m} \cdot \text{K)}$$

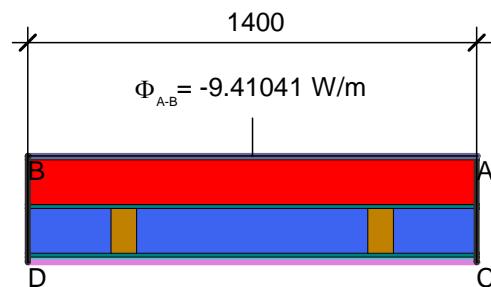
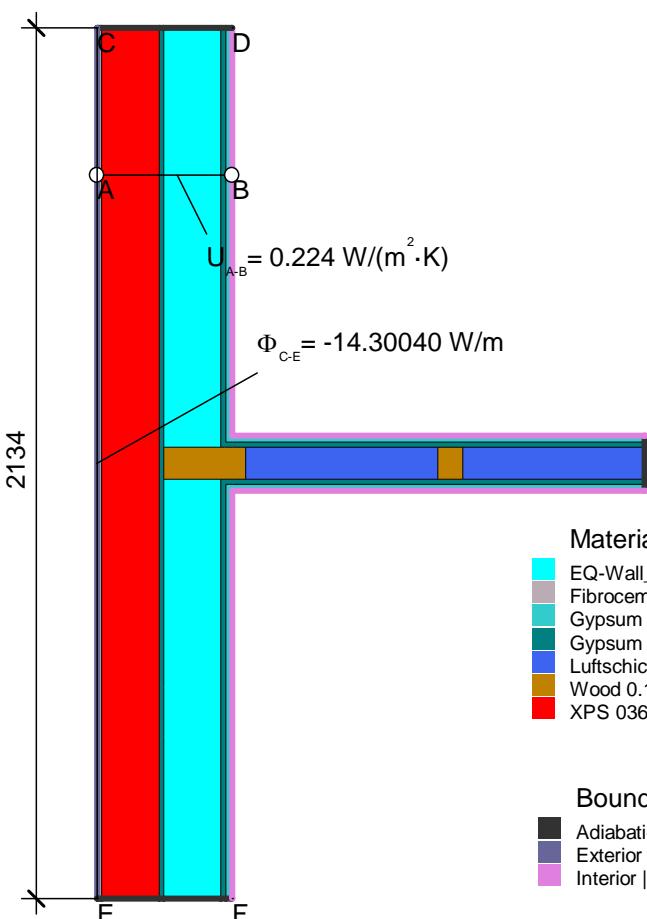


$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.410}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2 \cdot \text{K)}$$



Boundary Condition	$q[W/m^2]$	$\theta[^\circ C]$	$R[(m^2 \cdot K)/W]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet		-10.000	0.130	
fRsi: Interior Innen		20.000	0.250	



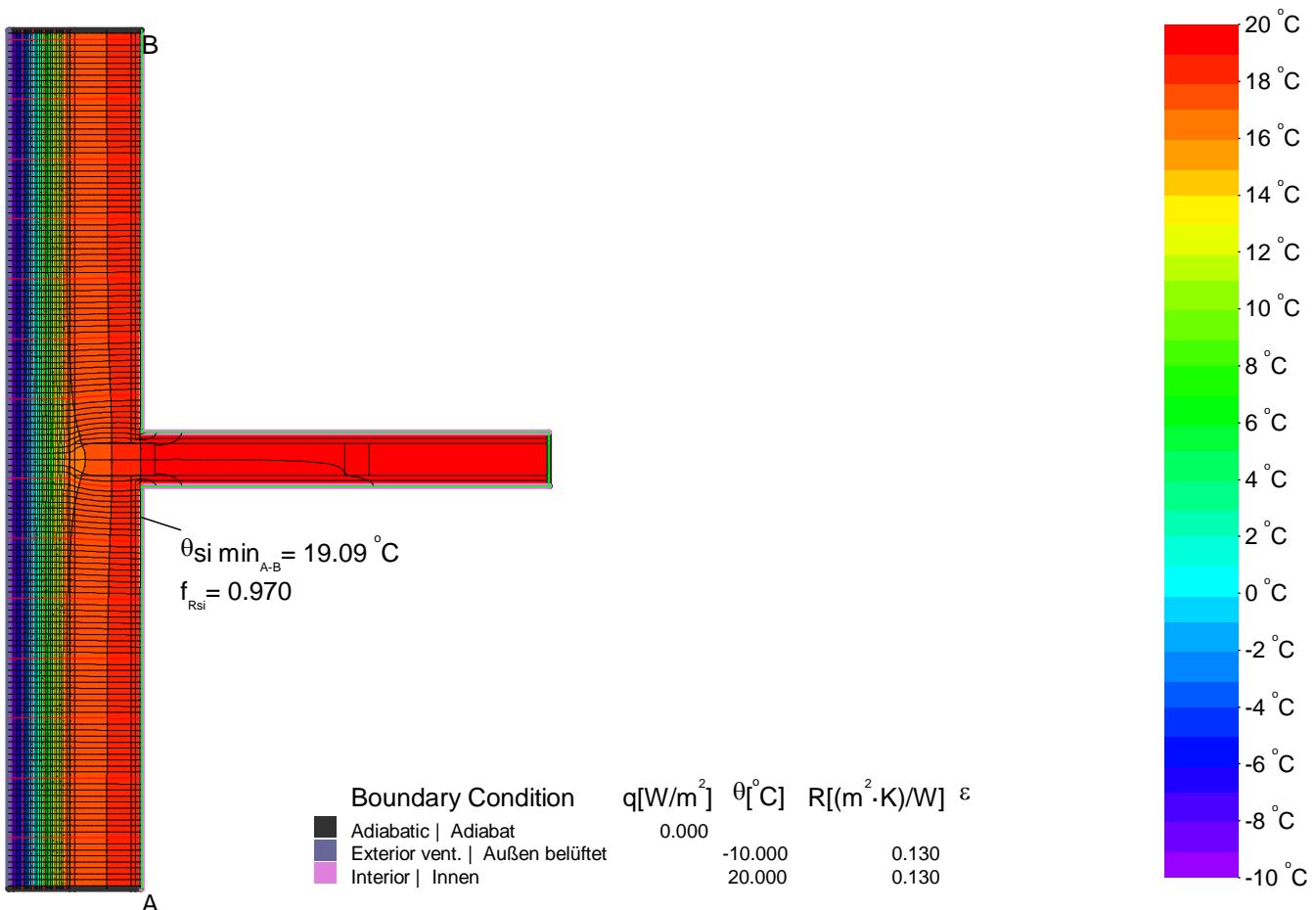


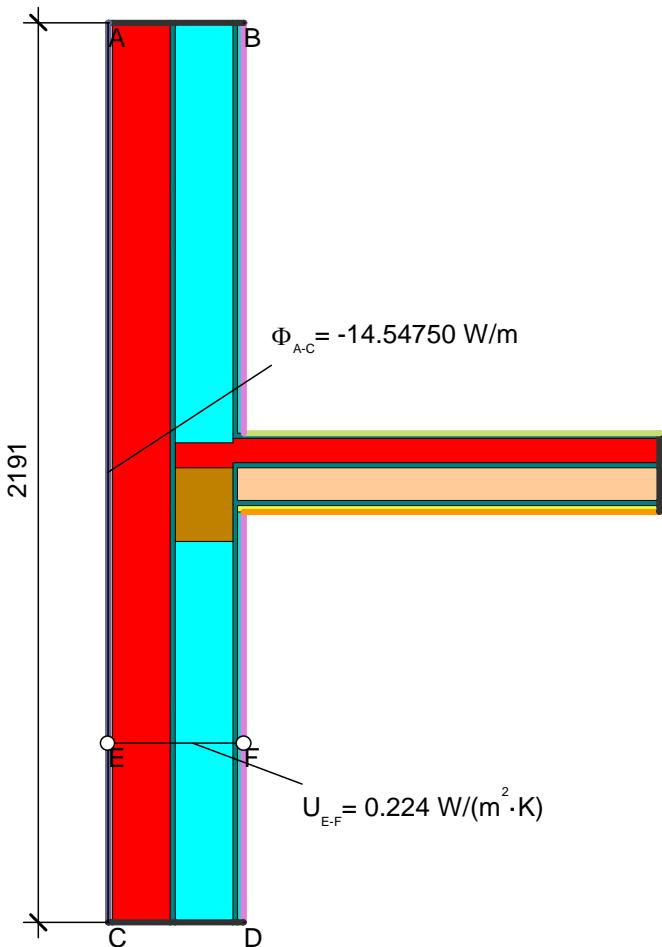
$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.410}{30.000 \cdot 1.400} = 0.224 \text{ W}/(\text{m}^2 \cdot \text{K})$$

Material	$\lambda[\text{W}/(\text{m} \cdot \text{K})]$	ε
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Luftschicht, ruhend, horizontal, Dicke: 140 mm (1)	0.778	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta [{}^\circ\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet		-10.000		0.130
Interior Innen		20.000		0.130

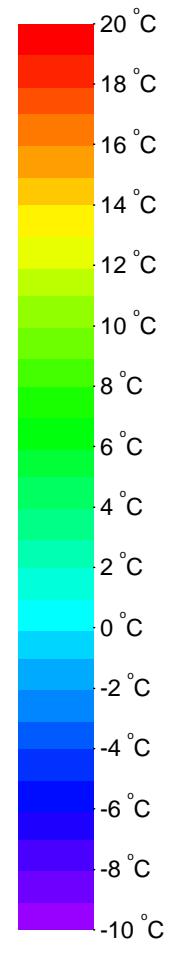
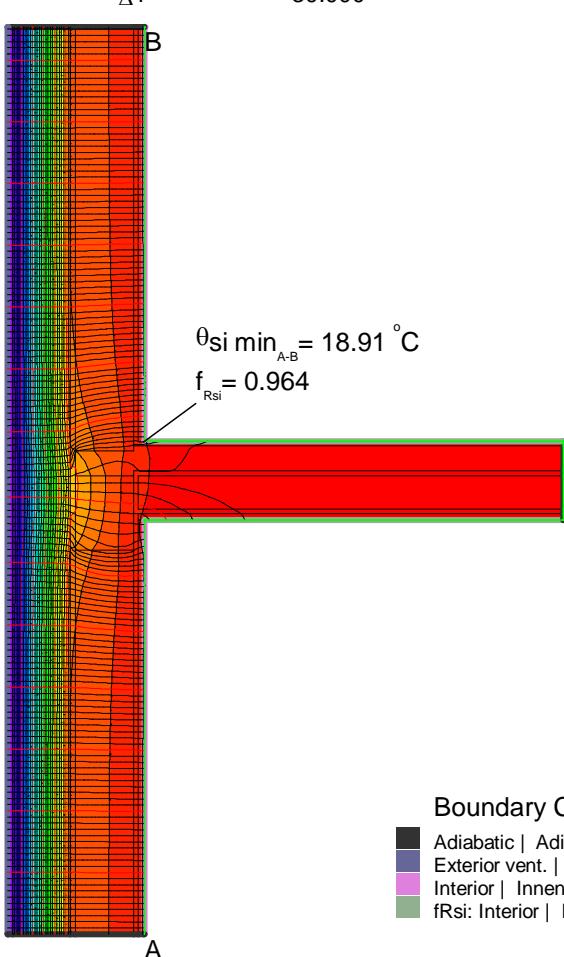
$$\psi_{C-E,*} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 = \frac{14.300}{30.000} - 0.224 \cdot 2.134 = -0.001 \text{ W}/(\text{m} \cdot \text{K})$$

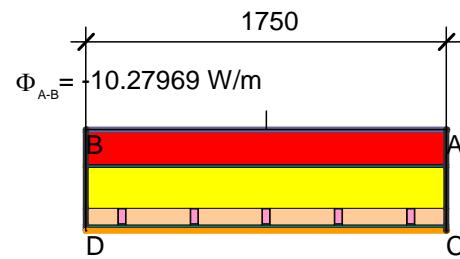
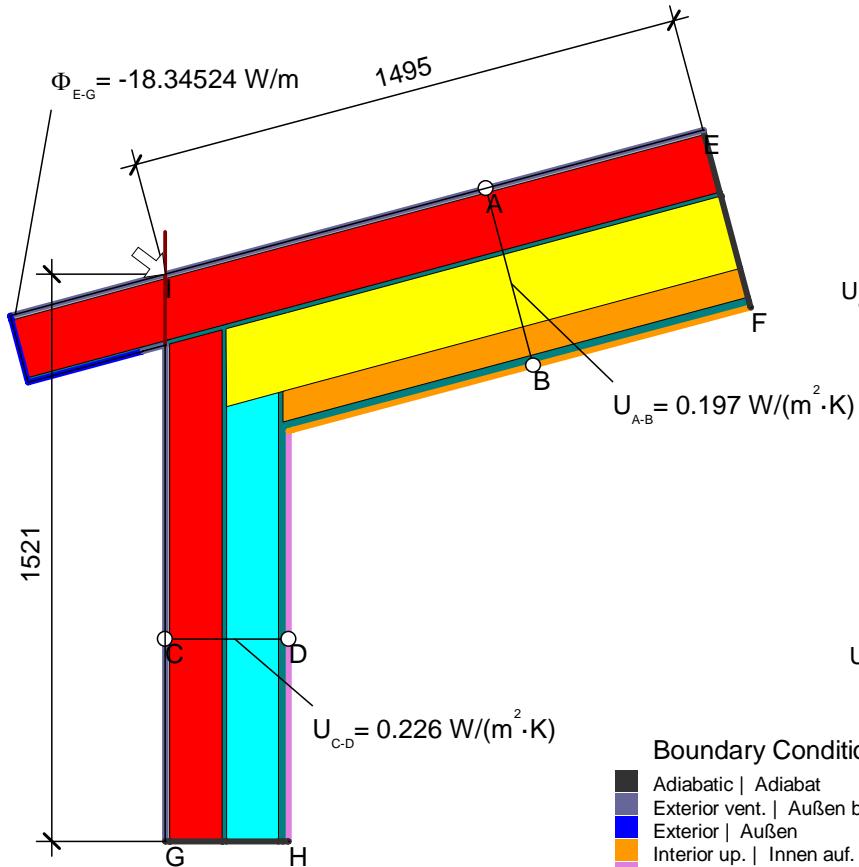




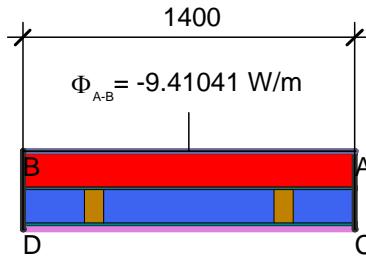
Material	$\lambda[\text{W}/(\text{m} \cdot \text{K})]$	ε
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board Gipskartonplatten 900 kg/m³ 10456	0.250	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Luftschicht, ruhend, aufwärts, Dicke: 80 mm	0.500	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[\text{°C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000			0.130
Int. flux down Innen abwärts	20.000			0.170
Interior up. Innen auf.	20.000			0.100
Interior Innen	20.000			0.130





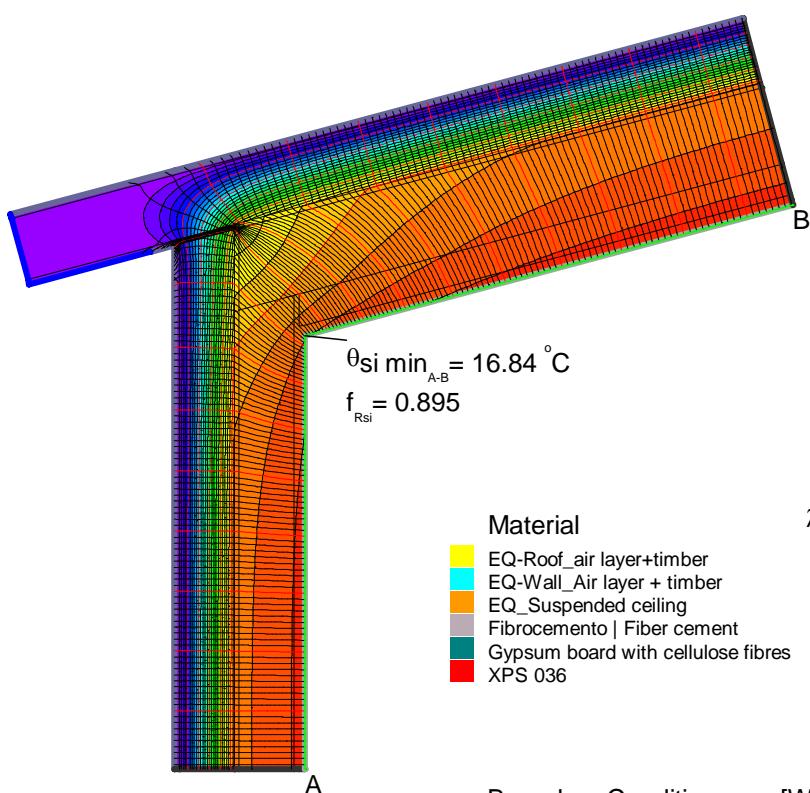
$$U_{eq\ A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{10.280}{30.000 \cdot 1.750} = 0.196 \text{ W/(m}^2\text{·K)}$$



$$U_{eq\ A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.410}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2\text{·K)}$$

Boundary Condition	$q[\text{W/m}^2]$	$\theta[{}^\circ\text{C}]$	$R[(\text{m}^2\text{-K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000		0.130	
Exterior Außen	-10.000		0.040	
Interior up. Innen auf.	20.000		0.100	
Interior Innen	20.000		0.130	

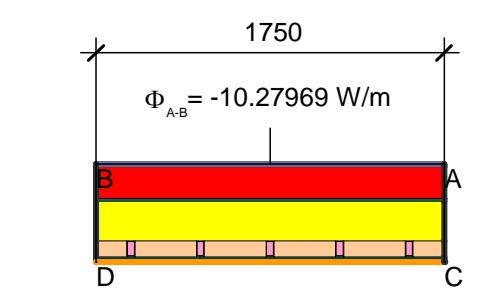
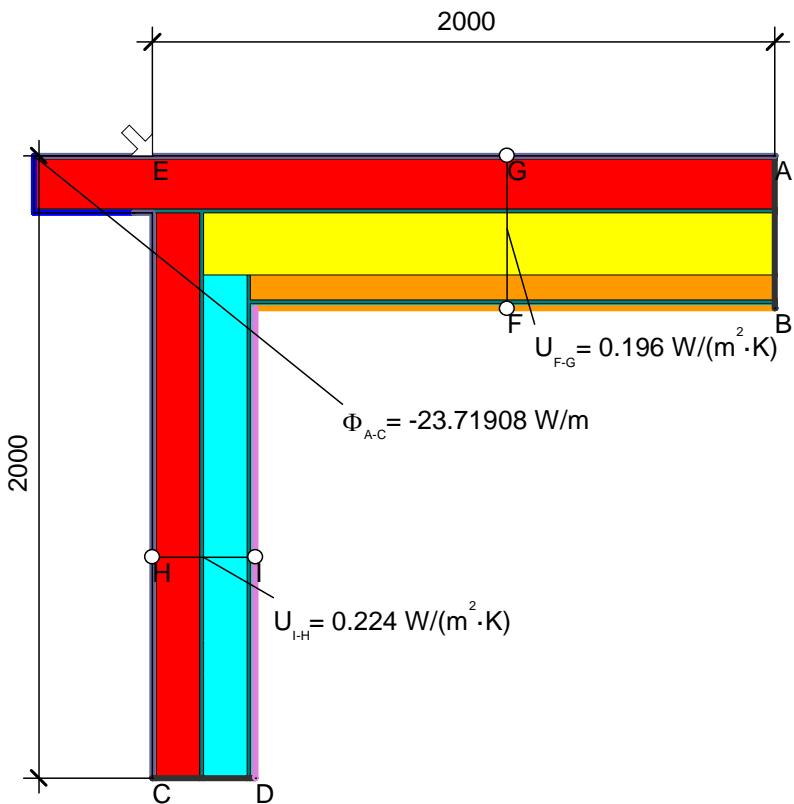
$$\psi_{E-I-G,\cdot} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{18.345}{30.000} - 0.196 \cdot 1.495 - 0.224 \cdot 1.521 = -0.022 \text{ W/(m·K)}$$



Material	$\lambda[\text{W/(m·K)}]$	ε
EQ-Roof_air layer+timber	0.920	0.900
EQ-Wall_Air layer + timber	0.666	0.900
EQ_Suspended ceiling	0.710	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board with cellulose fibres	0.669	0.900
XPS 036	0.036	0.900

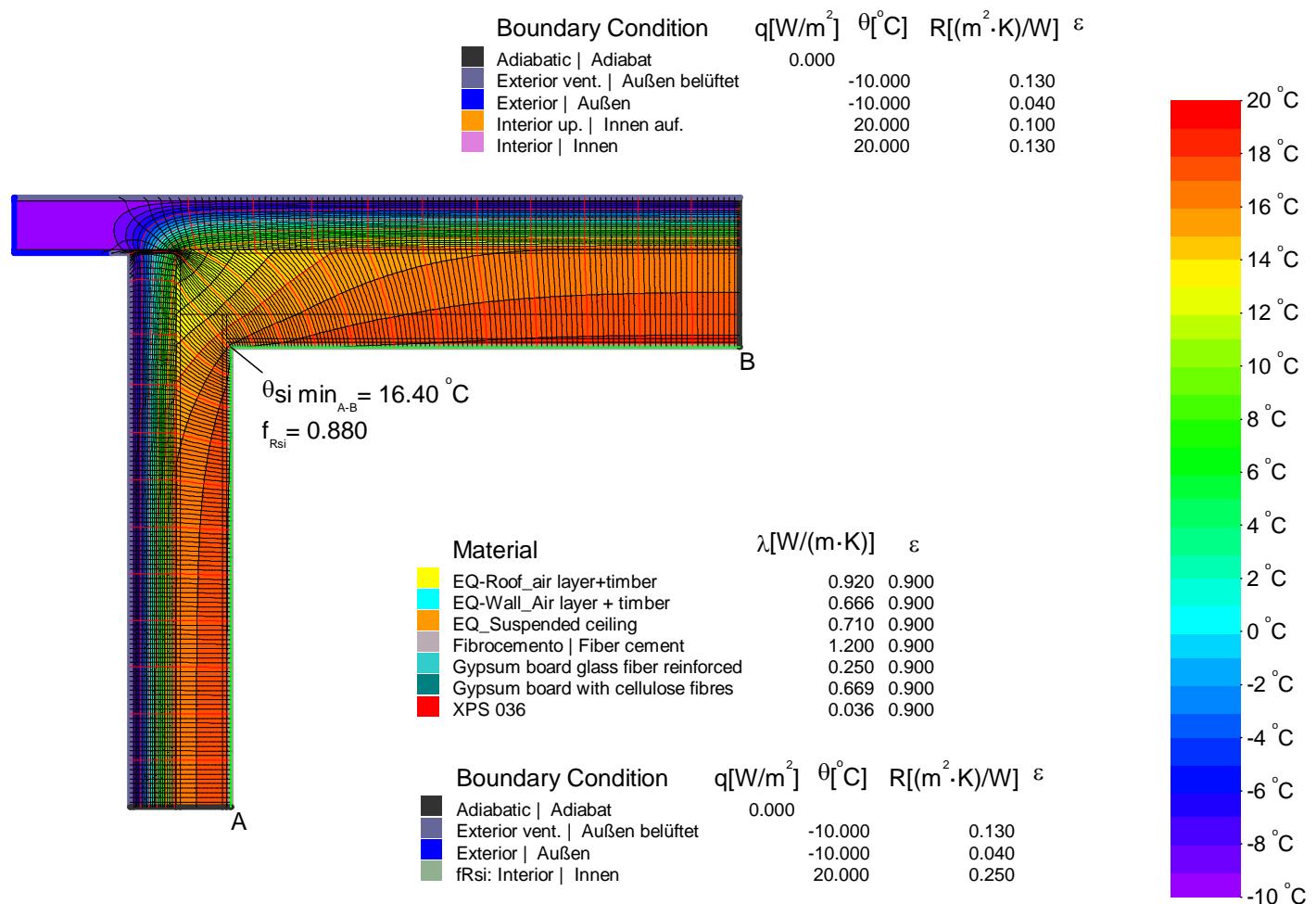
Boundary Condition	$q[\text{W/m}^2]$	$\theta[{}^\circ\text{C}]$	$R[(\text{m}^2\text{-K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000		0.130	
Exterior Außen	-10.000		0.040	
fRsi: Interior Innen	20.000		0.250	

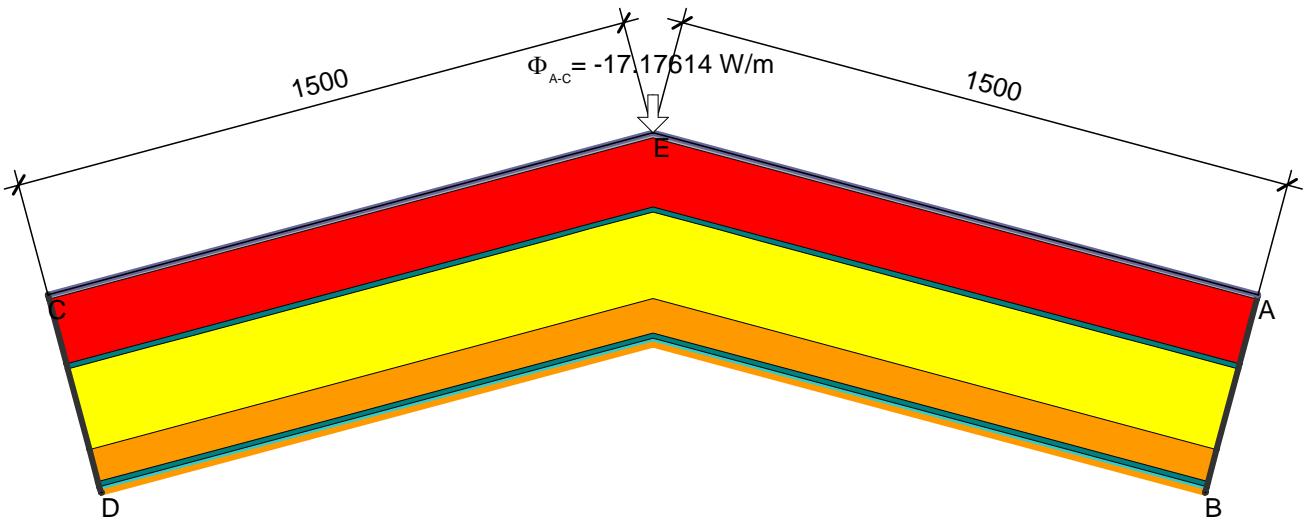




$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{10.280}{30.000 \cdot 1.750} = 0.196 \text{ W}/(\text{m}^2 \cdot \text{K})$$

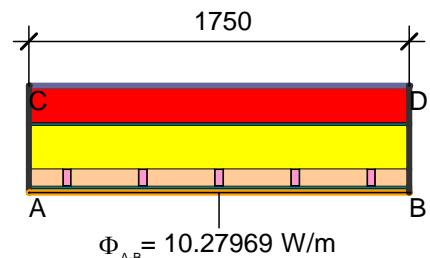
$$\psi_{A-E-C,-} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{23.719}{30.000} - 0.196 \cdot 2.000 - 0.224 \cdot 2.000 = -0.049 \text{ W}/(\text{m} \cdot \text{K})$$





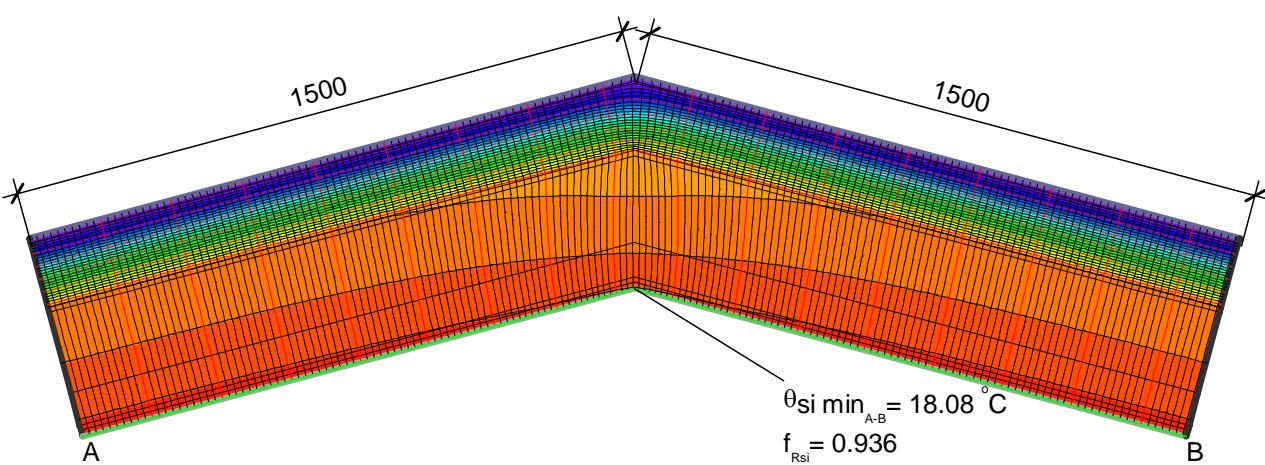
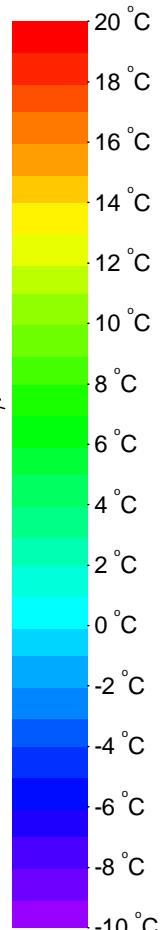
$$\psi_{A-E-C,*} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{17.176}{30.000} - 0.196 \cdot 1.500 - 0.196 \cdot 1.500 = -0.015 \text{ W/(m}\cdot\text{K)}$$

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^{\circ}\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000	-10.000	0.130	
Exterior vent. Außen belüftet		20.000	0.100	
Interior up. Innen auf.				



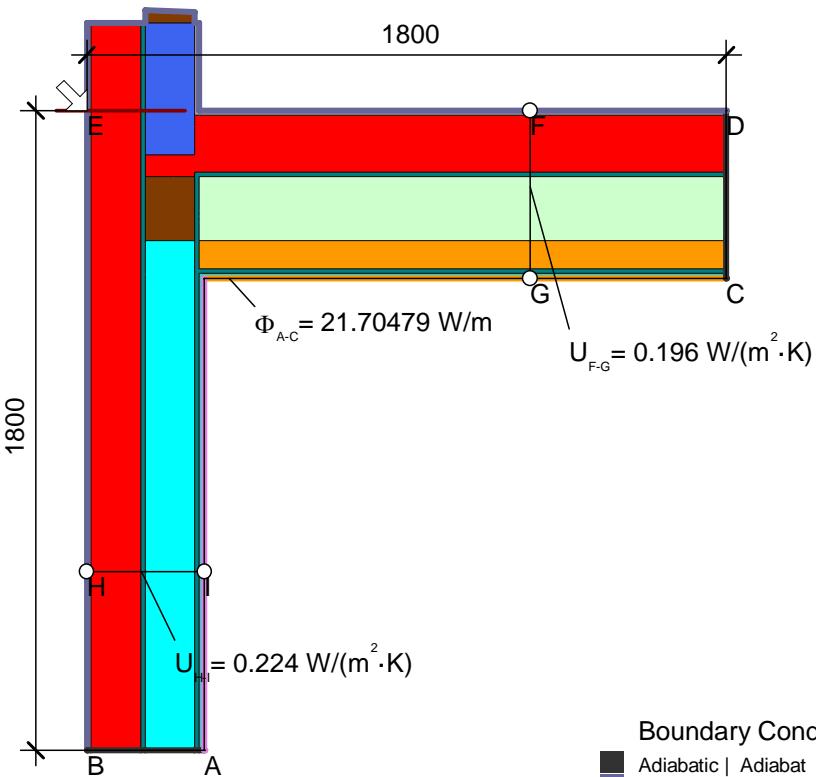
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EQ-Roof_air layer+timber	0.920	0.900
EQ_Suspended ceiling	0.710	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
XPS 036	0.036	0.900

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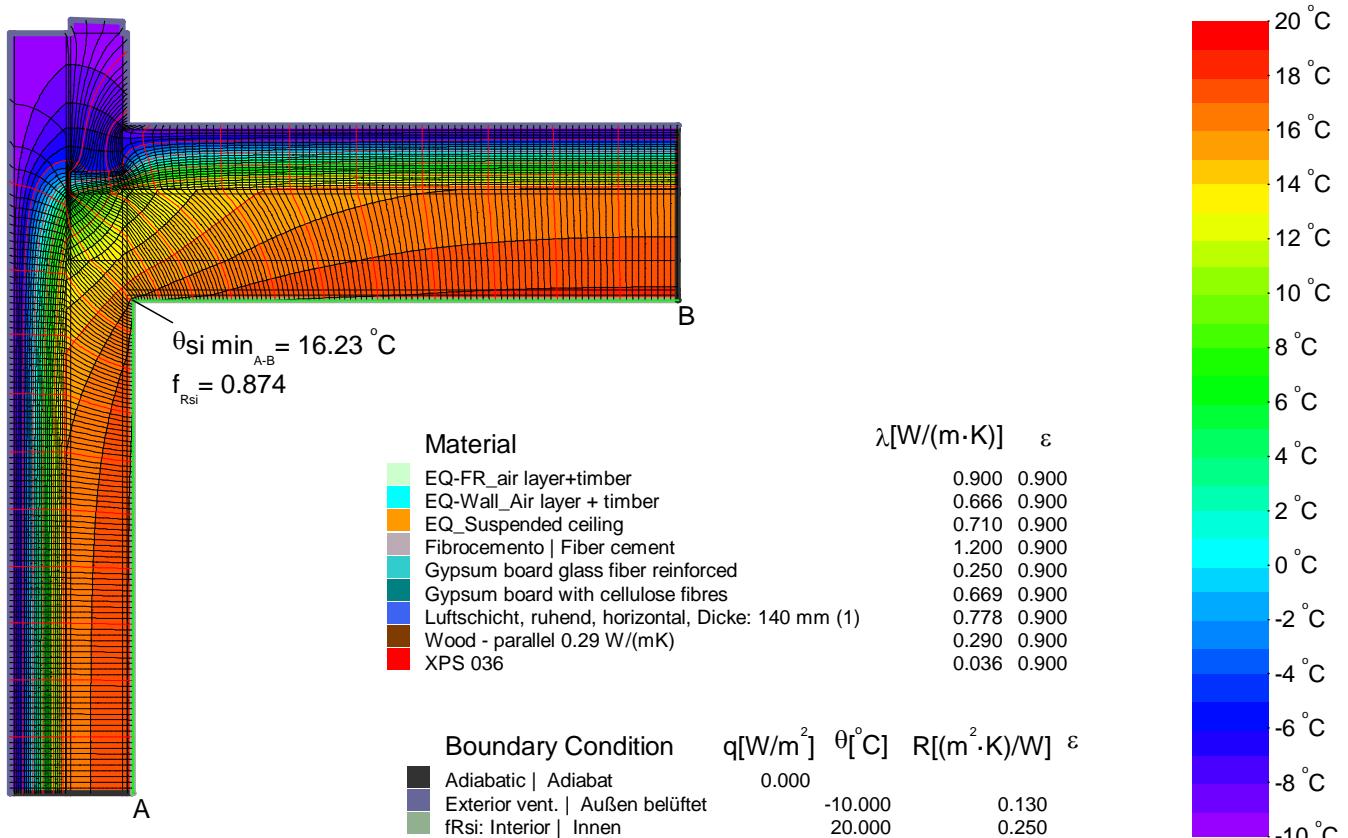
Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^{\circ}\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000	-10.000	0.130	
Exterior vent. Außen belüftet		20.000	0.250	

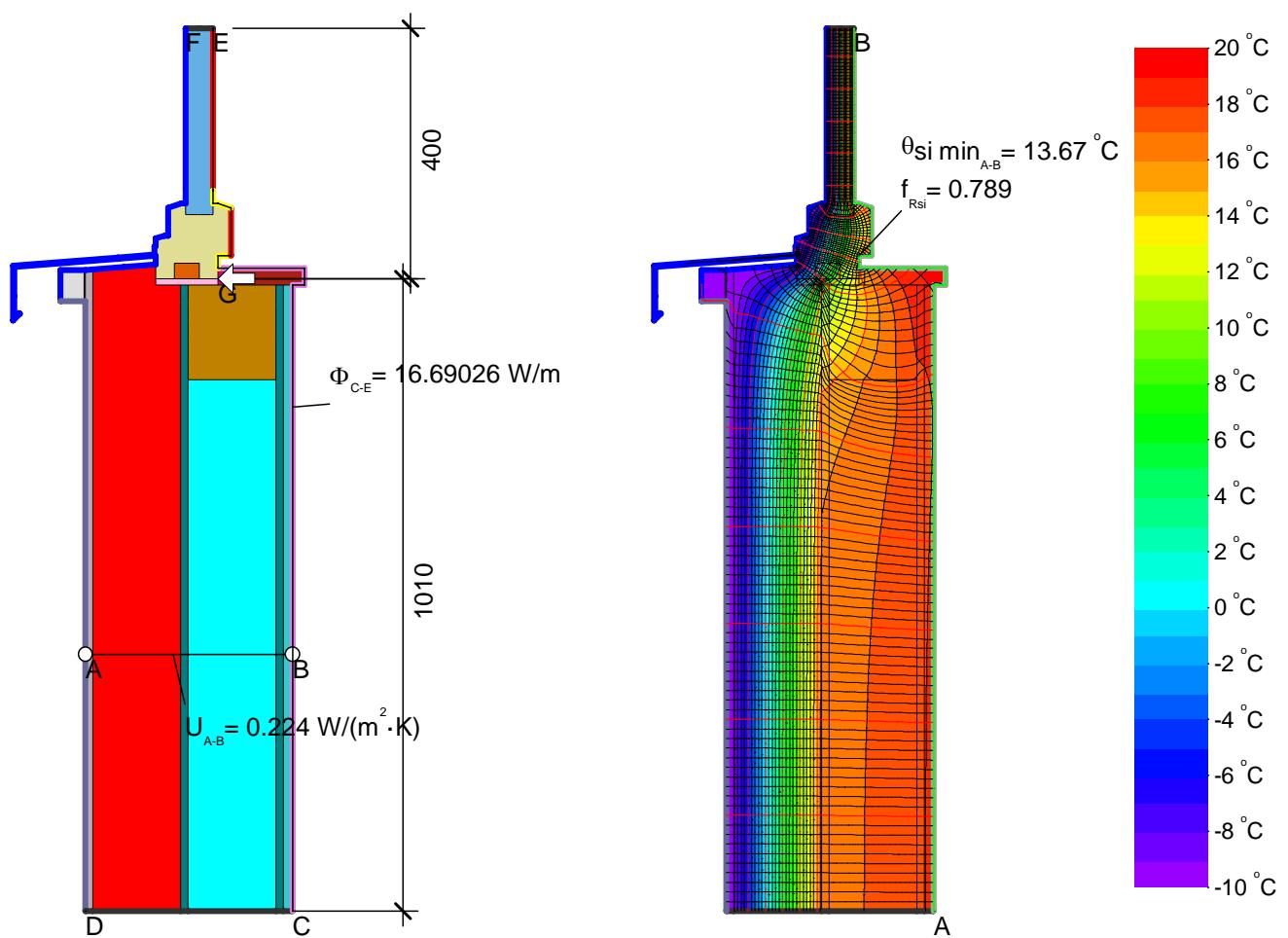




$U_{\text{eq A-B}} = \frac{\Phi}{\Delta T \cdot b} = \frac{10.482}{30.000 \cdot 1.750} = 0.200 \text{ W}/(\text{m}^2 \cdot \text{K})$																									
$U_{\text{eq A-B}} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.410}{30.000 \cdot 1.400} = 0.224 \text{ W}/(\text{m}^2 \cdot \text{K})$																									
<table border="1"> <thead> <tr> <th>Boundary Condition</th> <th>$q[\text{W}/\text{m}^2]$</th> <th>$\theta[^\circ\text{C}]$</th> <th>$R[(\text{m}^2 \cdot \text{K})/\text{W}]$</th> <th>$\varepsilon$</th> </tr> </thead> <tbody> <tr> <td>Adiabatic Adiabat</td> <td>0.000</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Exterior vent. Außen belüftet</td> <td>-10.000</td> <td></td> <td>0.130</td> <td></td> </tr> <tr> <td>Interior up. Innen auf.</td> <td>20.000</td> <td></td> <td>0.100</td> <td></td> </tr> <tr> <td>Interior Innen</td> <td>20.000</td> <td></td> <td>0.130</td> <td></td> </tr> </tbody> </table>	Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^\circ\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε	Adiabatic Adiabat	0.000				Exterior vent. Außen belüftet	-10.000		0.130		Interior up. Innen auf.	20.000		0.100		Interior Innen	20.000		0.130	
Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^\circ\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε																					
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Interior up. Innen auf.	20.000		0.100																						
Interior Innen	20.000		0.130																						

$$\psi_{A-E-C,-} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{21.705}{30.000} - 0.224 \cdot 1.800 - 0.200 \cdot 1.800 = -0.039 \text{ W}/(\text{m} \cdot \text{K})$$

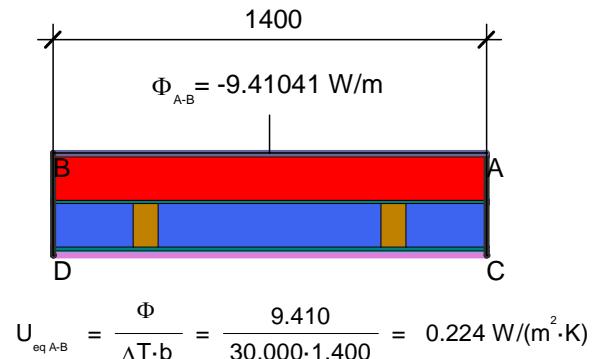




$$\psi_{C-G-E, \cdot} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - \frac{\Phi_2}{\Delta T} = \frac{16.690}{30.000} - 0.224 \cdot 1.010 - \frac{9.453}{30.000} = 0.015 \text{ W/(m·K)}$$

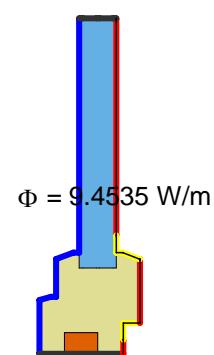
Material	$\lambda [\text{W}/(\text{m} \cdot \text{K})]$	ε
Aluminum Aluminium 10456	160.000	0.900
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Hardwood Hartholz 0.18 700 kg/m³ 10456	0.180	0.900
Insulation Wärmedämmung 050	0.050	0.900
PU in-situ foam PU-Ortschaum 040	0.040	0.900
Panel Maske	0.035	0.900
Silicone Silikon	0.350	0.900
Softwood, OSB Weichholz, OSB ISO 10456	0.130	0.900
Unvent. cavity unbel. Hohlr. *		
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

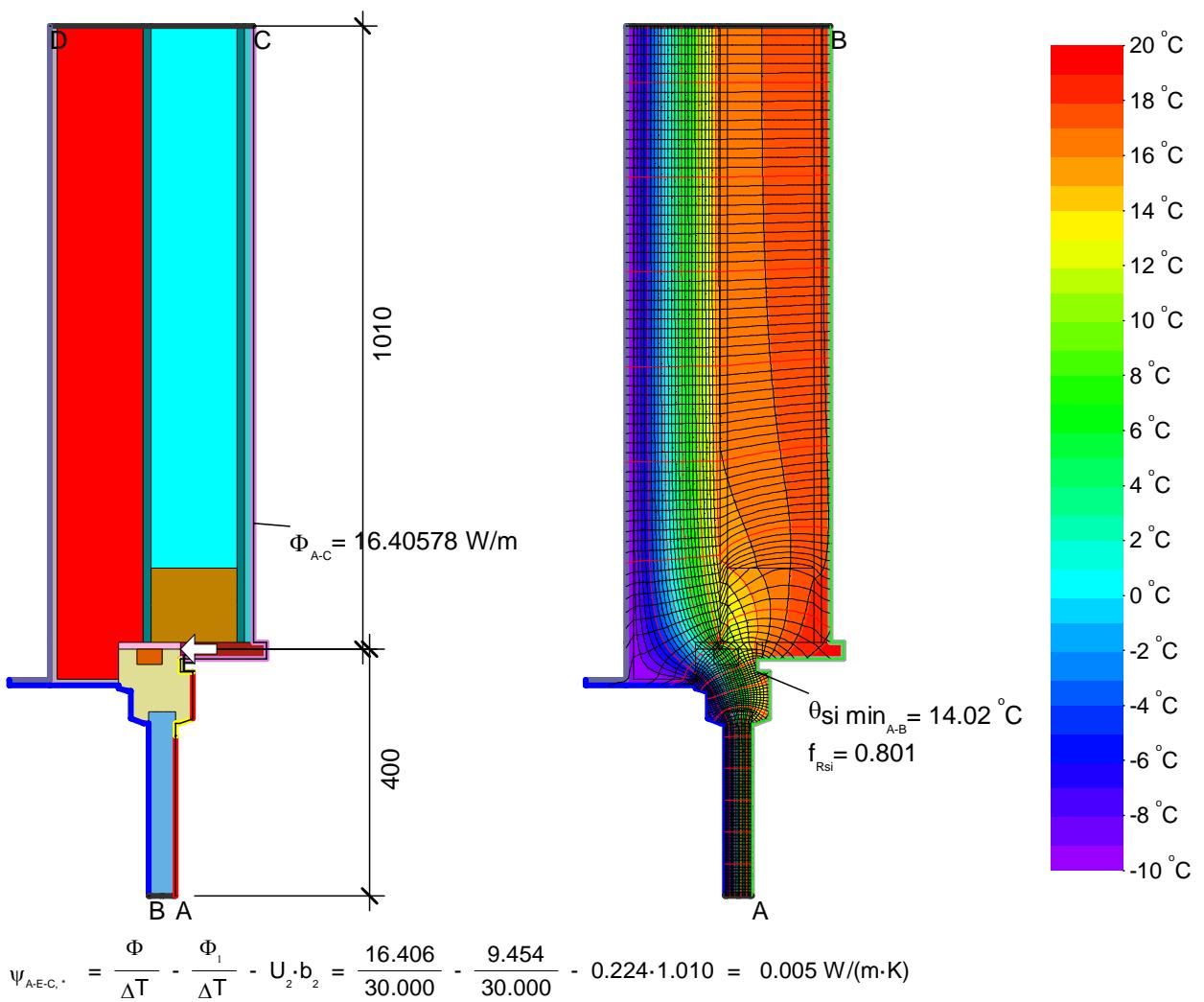
* EN ISO 10077-2:2017, 6.4.3



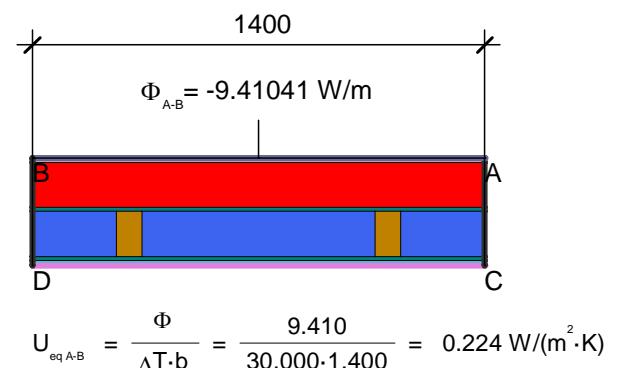
$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.410}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2 \cdot \text{K)}$$

Boundary Condition	$q [\text{W}/\text{m}^2]$	$\theta [{}^\circ\text{C}]$	$R [(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000	0.130		
Exterior Außen	-10.000	0.040		
Interior Innen	20.000	0.130		
Interior, frame, normal	20.000	0.130		
Interior, frame, reduced	20.000	0.200		
e 0,9 Cavity Hohlraum			0.900	

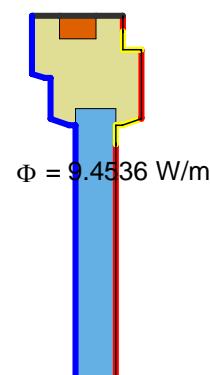


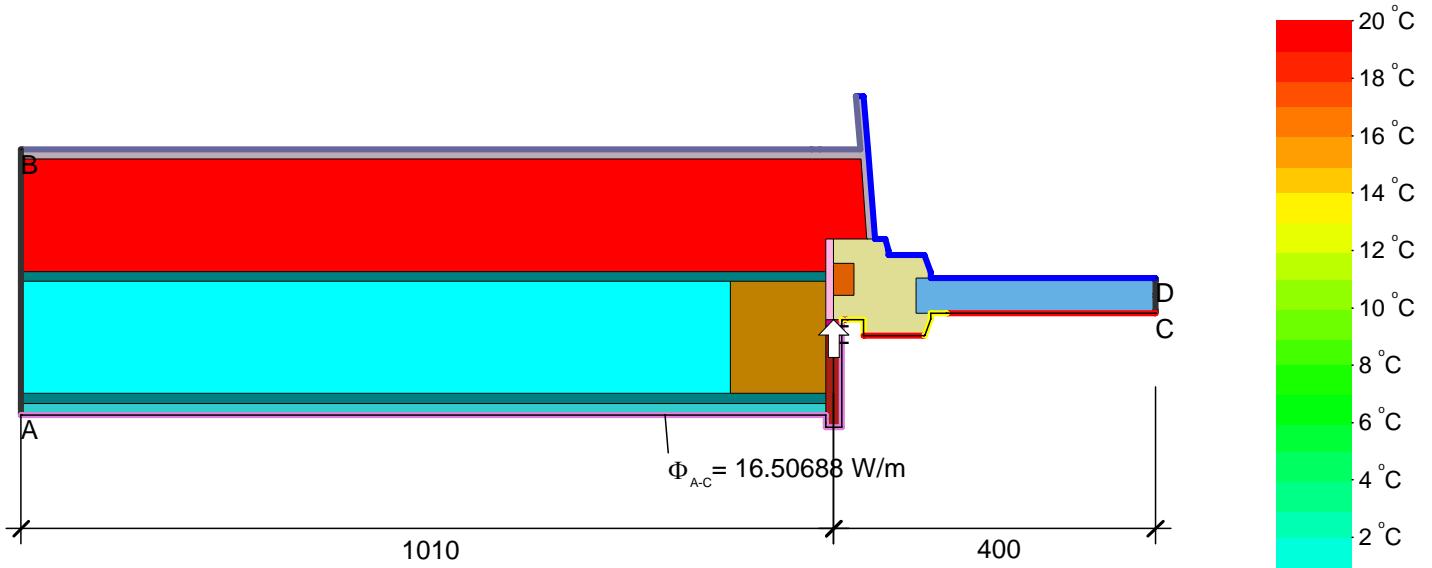


Material	$\lambda[\text{W}/(\text{m}\cdot\text{K})]$	ε
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Hardwood I Hartholz 0.18 700 kg/m³ 10456	0.180	0.900
Insulation I Wärmedämmung 050	0.050	0.900
PU in-situ foam I PU-Ortschaum 040	0.040	0.900
Panel I Maske	0.035	0.900
Silicone I Silikon	0.350	0.900
Softwood, OSB I Weichholz, OSB ISO 10456	0.130	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

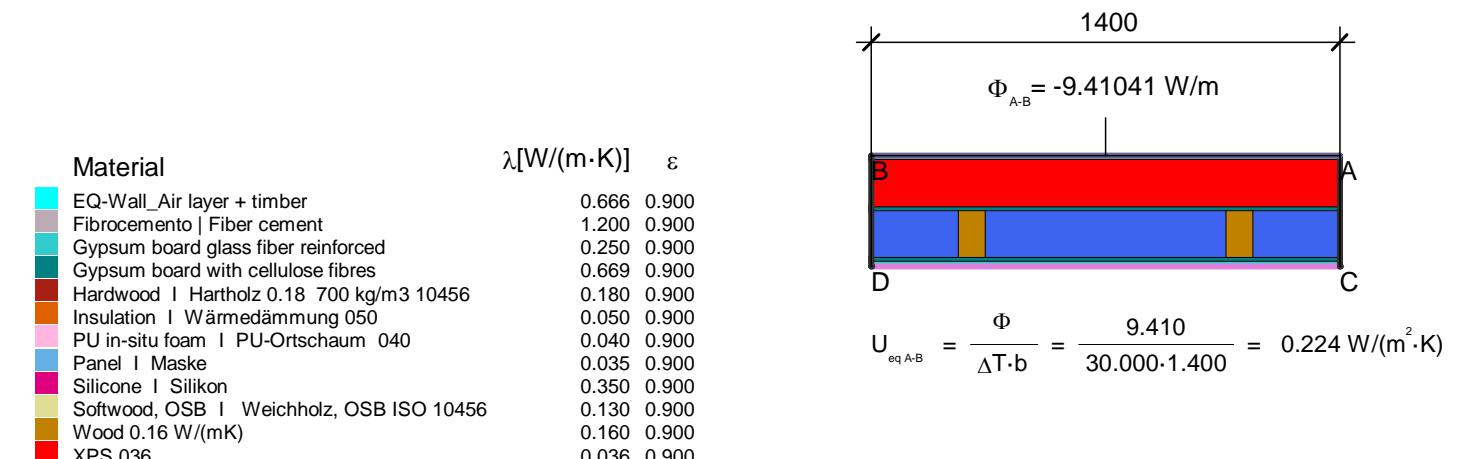
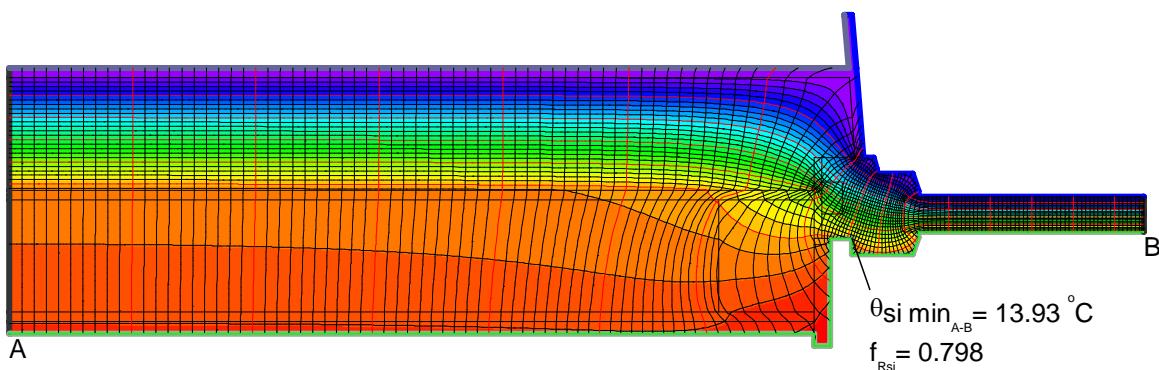


Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[{}^{\circ}\text{C}]$	$R[(\text{m}^2\cdot\text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Aussen Standard		-10.000	0.040	
Exterior vent. Außen belüftet		-10.000	0.130	
Interior Innen		20.000	0.130	
Interior, frame, normal		20.000	0.130	
Interior, frame, reduced		20.000	0.200	



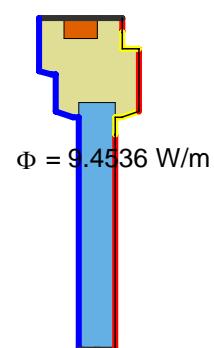


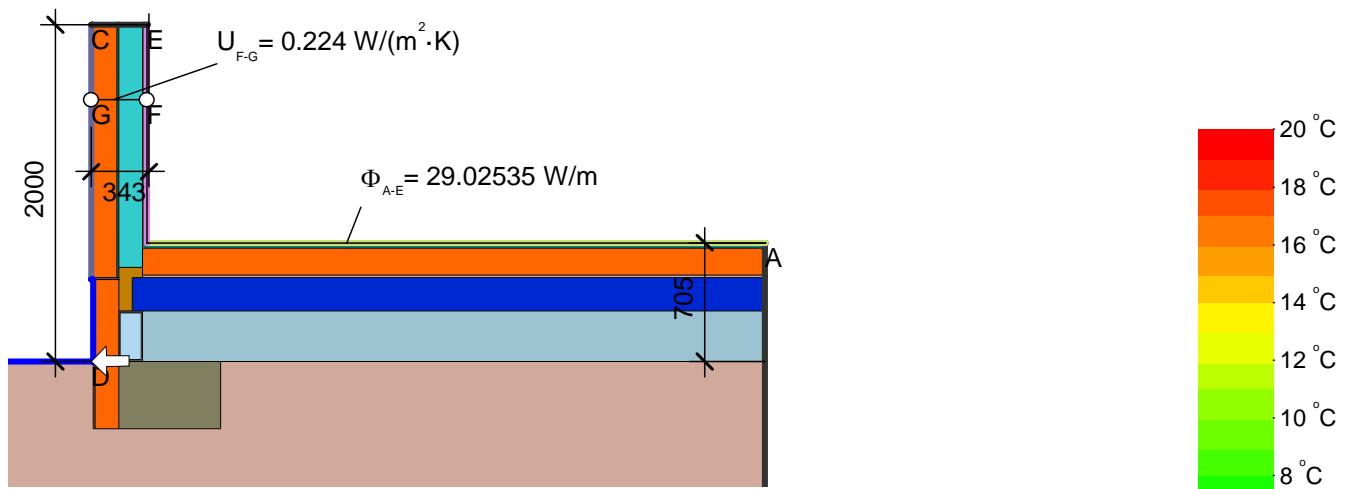
$$\psi_{A-E-C,-} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - \frac{\Phi_2}{\Delta T} = \frac{16.507}{30.000} - 0.224 \cdot 1.010 - \frac{9.454}{30.000} = 0.009 \text{ W/(m}\cdot\text{K)}$$



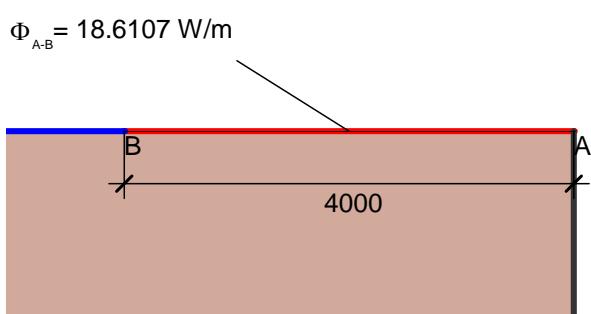
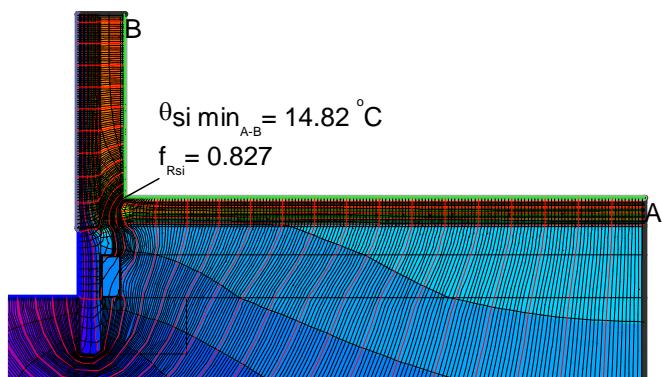
Material	$\lambda [\text{W}/(\text{m}\cdot\text{K})]$	ϵ
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Hardwood Hartholz 0.18 700 kg/m³ 10456	0.180	0.900
Insulation Wärmedämmung 050	0.050	0.900
PU in-situ foam PU-Ortschaum 040	0.040	0.900
Panel Maske	0.035	0.900
Silicone Silikon	0.350	0.900
Softwood, OSB Weichholz, OSB ISO 10456	0.130	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

Boundary Condition	$q [\text{W}/\text{m}^2]$	$\theta [{}^{\circ}\text{C}]$	$R [(\text{m}^2 \cdot \text{K})/\text{W}]$	ϵ
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet		-10.000	0.130	
Exterior Außen		-10.000	0.040	
Innen Fensterrahmen Reduziert		20.000	0.200	
Innen Fensterrahmen Standard		20.000	0.130	
Interior Innen		20.000	0.130	

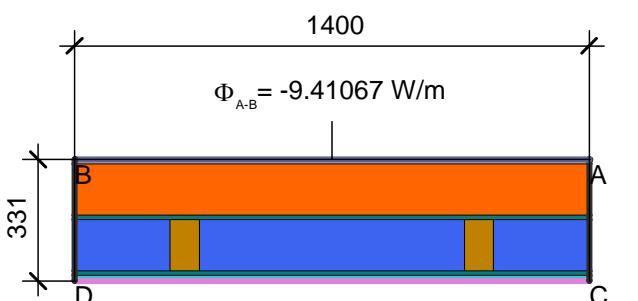




$$\psi_{A-D-E, \dots} = \frac{\Phi}{\Delta T} - \frac{\Phi_1}{\Delta T} - U_2 \cdot b_2 = \frac{29.025}{30.000} - \frac{18.611}{30.000} - 0.224 \cdot 2.000 = -0.101 \text{ W}/(\text{m} \cdot \text{K})$$



Material	$\lambda [\text{W}/(\text{m} \cdot \text{K})]$	ϵ
Aluminum Aluminium 10456	160.000	0.900
Concrete, 1% Steel Beton, 1% Stahl ISO 10456	2.300	0.900
EPDM	0.250	0.900
EQ-Wall_Air layer + timber	0.656	0.900
Fibrocemento Fiber cement	1.200	0.900
Ground Erdreich	2.000	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Luftschicht, ruhend, horizontal, Dicke: 280 mm	1.556	0.900
Luftschicht, schwach belüftet, aufwärts, Dicke: 200 mm	2.500	0.900
Luftschicht, schwach belüftet, aufwärts, Dicke: 300 mm	3.750	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

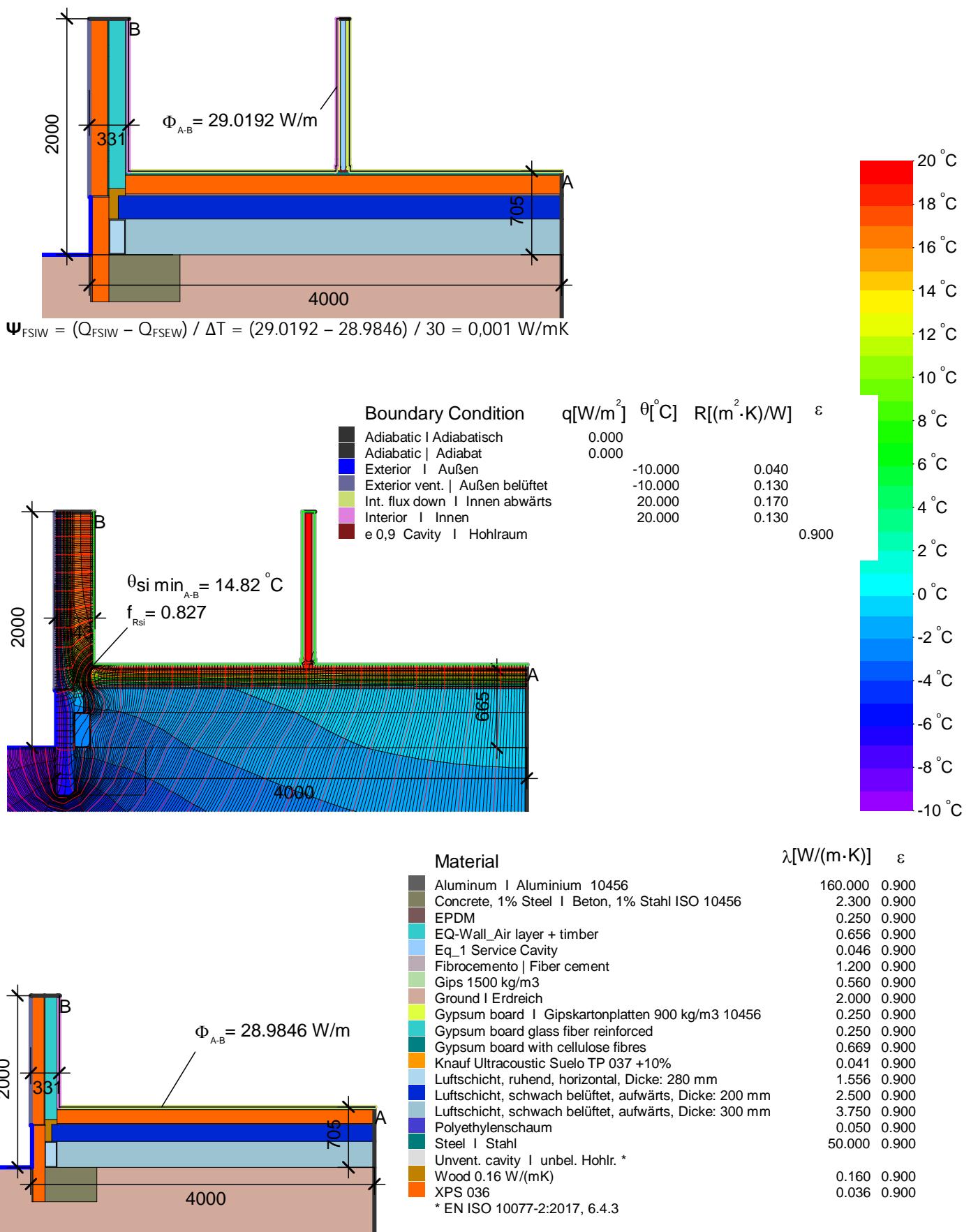


$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.411}{30.000 \cdot 1.400} = 0.224 \text{ W}/(\text{m}^2 \cdot \text{K})$$

Boundary Condition	$q [\text{W}/\text{m}^2]$	$\theta [{}^\circ\text{C}]$	$R [(\text{m}^2 \cdot \text{K})/\text{W}]$	ϵ
Adiabatic	0.000			
Adiabatic Adiabat	0.000			
Exterior Außen	-10.000		0.040	
Exterior vent. Außen belüftet	-10.000		0.130	
Int. flux down Innen abwärts	20.000		0.170	
Interior Innen	20.000		0.130	

Boundary Condition	$q [\text{W}/\text{m}^2]$	$\theta [{}^\circ\text{C}]$	$R [(\text{m}^2 \cdot \text{K})/\text{W}]$	ϵ
Adiabatic	0.000			
Adiabatic Adiabat	0.000			
Exterior Außen	-10.000		0.040	
Exterior vent. Außen belüftet	-10.000		0.130	
fRsi: Interior Innen	20.000		0.250	



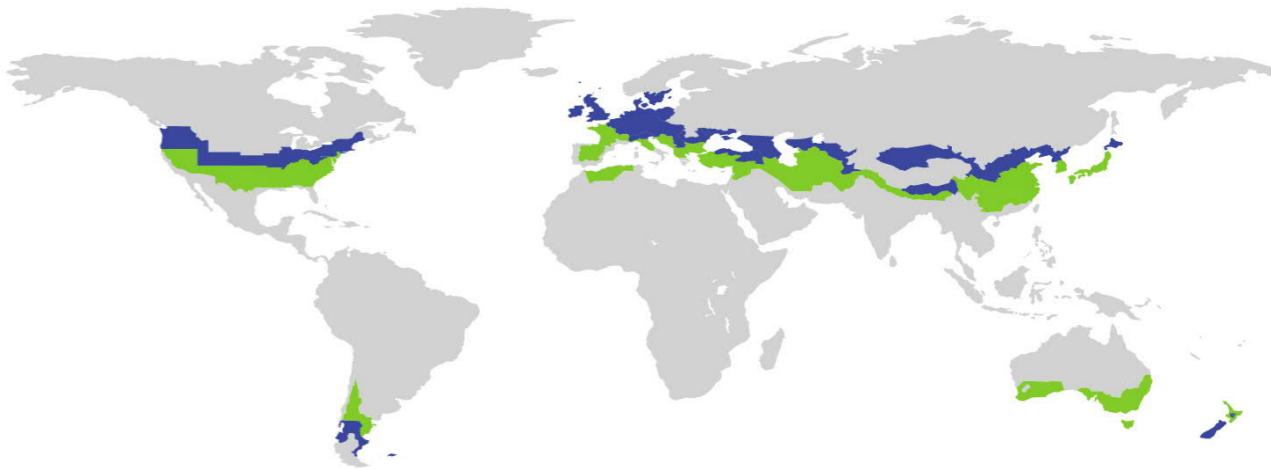


CERTIFICATE

Certified Passive House Component

ID: 1598cs04 valid until 31. December 2021

Passive House Institute
Dr. Wolfgang Feist
64342 Darmstadt
GERMANY



Category	Construction system Lightweight timber construction
Manufacturer	Thermochip SLU Carballeda de Valdeorras (Ourense) España
Product name	Thermochip HOUSING SATE-WALL

This certificate for the warm, temperate climate zone was awarded based on the following criteria

Hygiene criterion

The minimum temperature factor of the interior surfaces is

$f_{Rsi=0,25m^2K/W} \geq 0.65$

Comfort criterion

The U-value of the installed windows is

$U_{w,i} \leq 1.05 \text{ W}/(\text{m}^2\text{K})$

Efficiency criteria

Heat transfer coefficient of building envelope

$U^*f_{PHI} \leq 0.30 \text{ W}/(\text{m}^2\text{K})$

Temperature factor of opaque junctions

$f_{Rsi=0,25m^2K/W} \geq 0.82$

Thermal bridge-free design for key connection details

$\Psi \leq 0.01 \text{ W}/(\text{mK})$

An airtightness concept for all components and connection details was provided



Opaque building envelope

With the Thermochip HOUSING Construction System the wintertime thermal insulation of buildings can be ensured. The system is constructed out of timber studs, beams and two sandwich panels. The external sandwich panel (12/80/12 mm) comprises a board of fibre cement to the outside, a core of XPS ($\lambda=0.036$ W/mK) and internal composite board with cellulose fibres. The internal sandwich panel (12/60/12 mm) uses the same core of XPS but two composite boards with cellulose fibres. The assembly is thereby insulated both to the outside and inside.

For the purpose of certification, a three-dimensional simulation was carried out to determine the effect of the timber roof beams which penetrates the external wall at eaves level.

The certification does not take into account point thermal bridges caused by structural columns or e.g. balcony connections, which must be assessed separately. As investigated, the system is deemed suitable for passive houses in the warm-temperate climate zone, as the regular U-values of the exterior components are below 0,25 W/m²K and the connections meet the criteria of 'thermal bridge free'. The surface temperature of all connections (with the

Explanatory notes

The Passive House Institute has defined international component criteria for seven climate zones based on hygiene, comfort and affordability criteria. In principle, components which have been certified for climate zones with higher requirements may also be used in climates with less stringent requirements. Their use might make economic sense in certain circumstances.

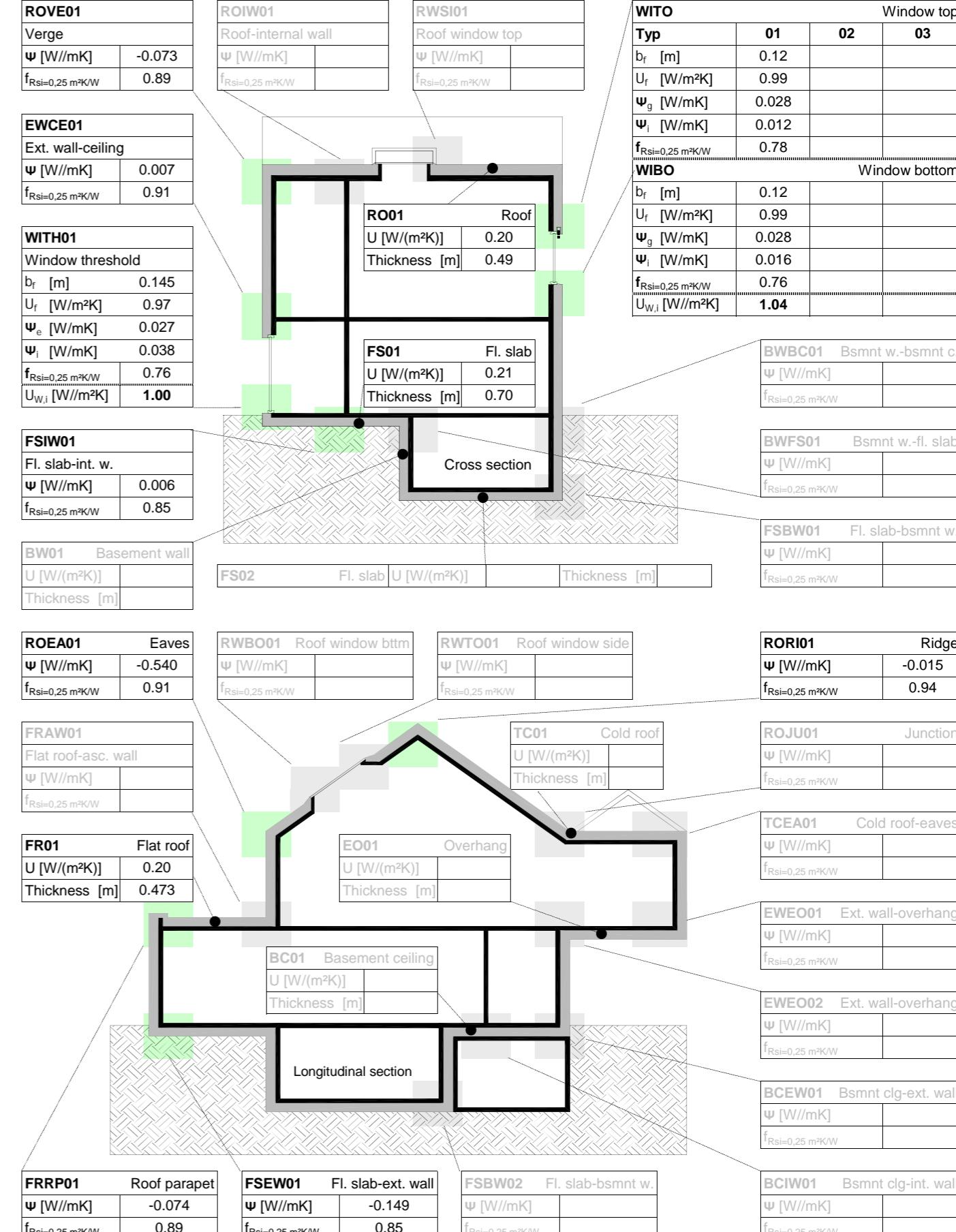
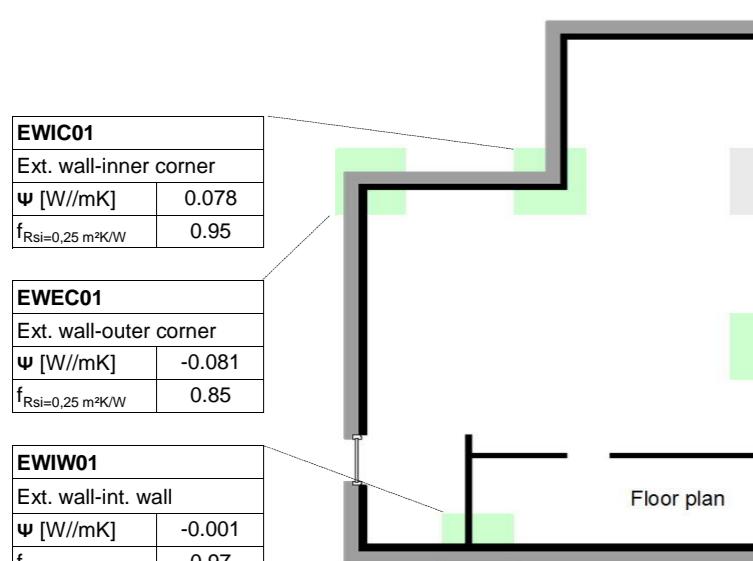
Thermal bridge not calculated
Criteria achieved

Windows

For the purposes of certification a standard passive house window ($U_w = 1,00$ W/m²K with $U_g = 0,90$ W/m²K) was used. The overall U-value of the installed window of standard size (1,23 m wide by 1,48 m tall) should be no more than 0,05 W/m²K greater than the U_w to ensure occupant comfort - this criteria is met in this instance.

Airtightness concept

Airtightness of the system is achieved in the following way: windows and doors are installed with permanently elastic sealing materials and suitable airtight connection membranes and profiles. The airtight layer of the wall is the interior gypsum fibre board of the outer panel. In the roof and floor slab where only one sandwich panel is used, the air tight layer remains on the interior gypsum fibre board of the panel. Joints between panels and connections with other building elements are sealed with Soudal Soudatight SP airtight paint.

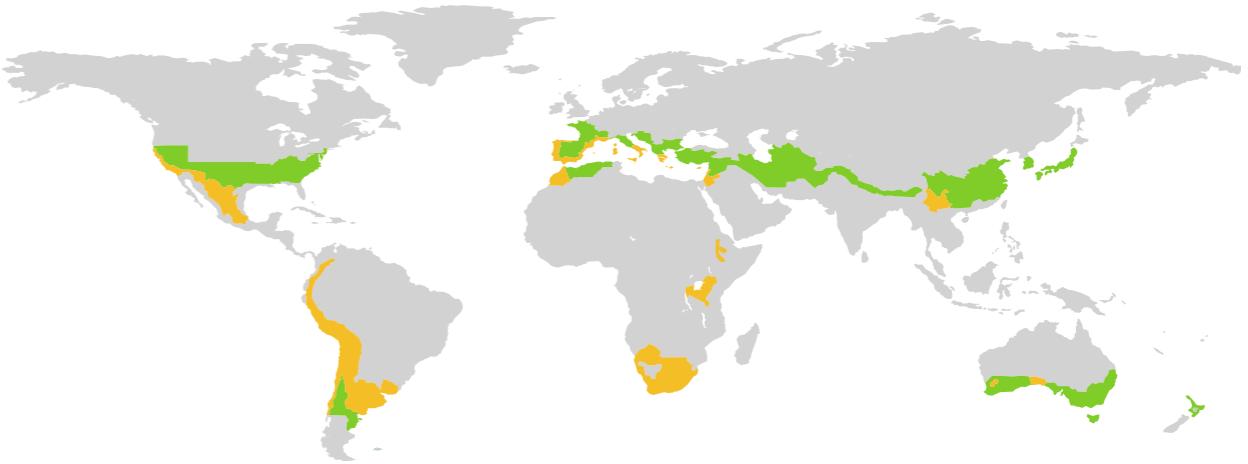


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The minimum temperature factor of the interior surfaces is

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Comfort criterion

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Efficiency criteria

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Temperature factor of opaque junctions

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Thermal bridge-free design for key connection details

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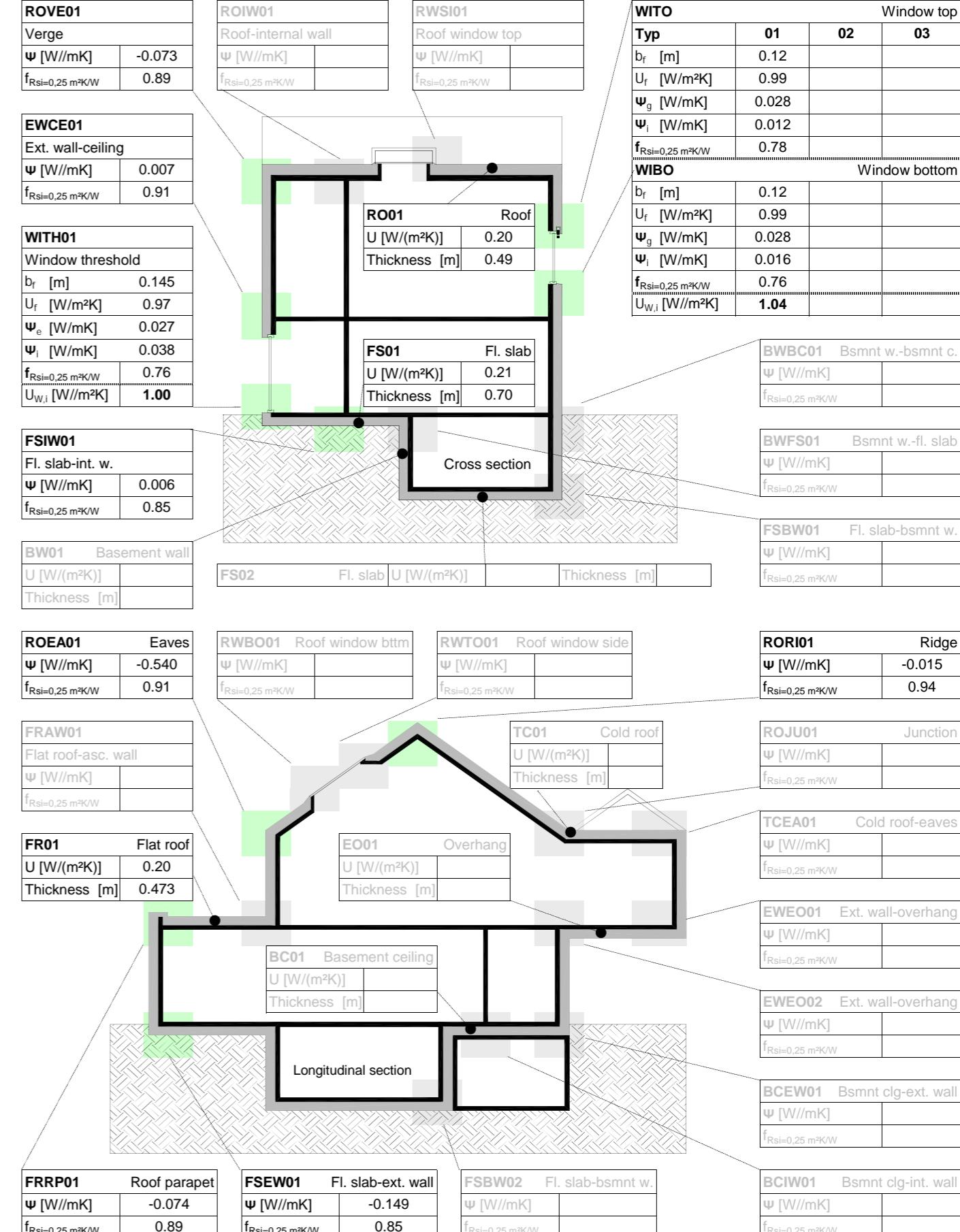
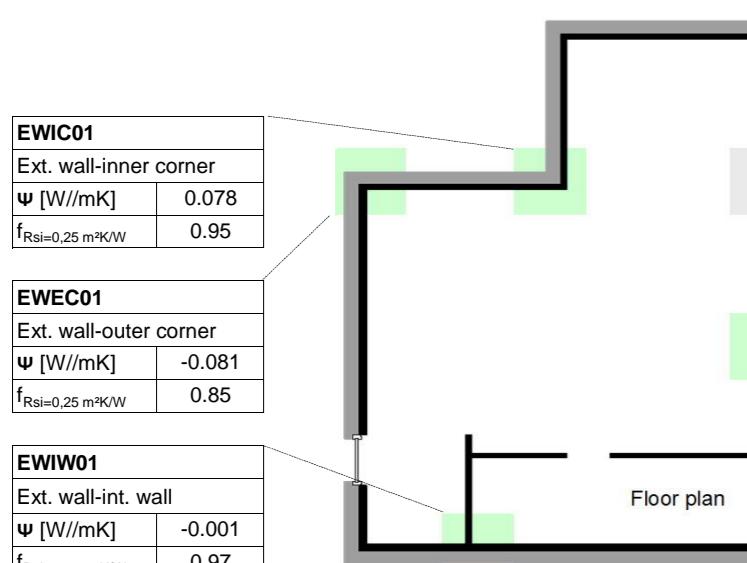
Thermal bridge not calculated
Criteria achieved

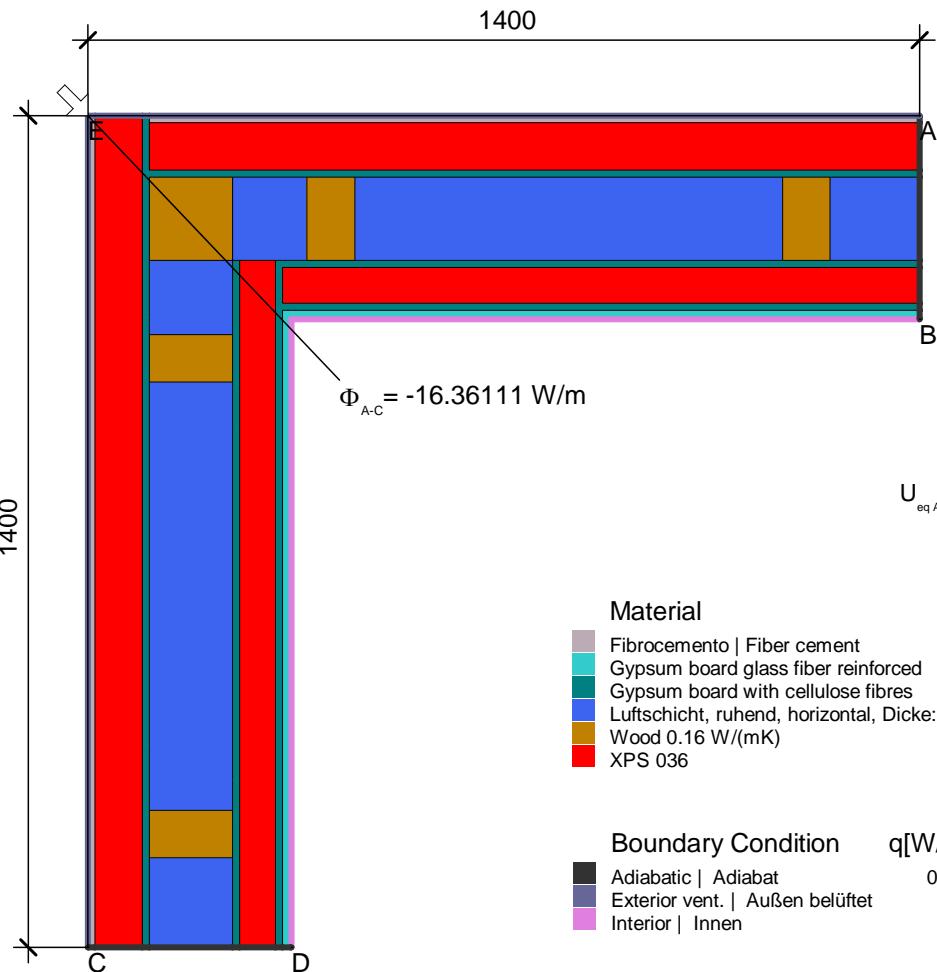
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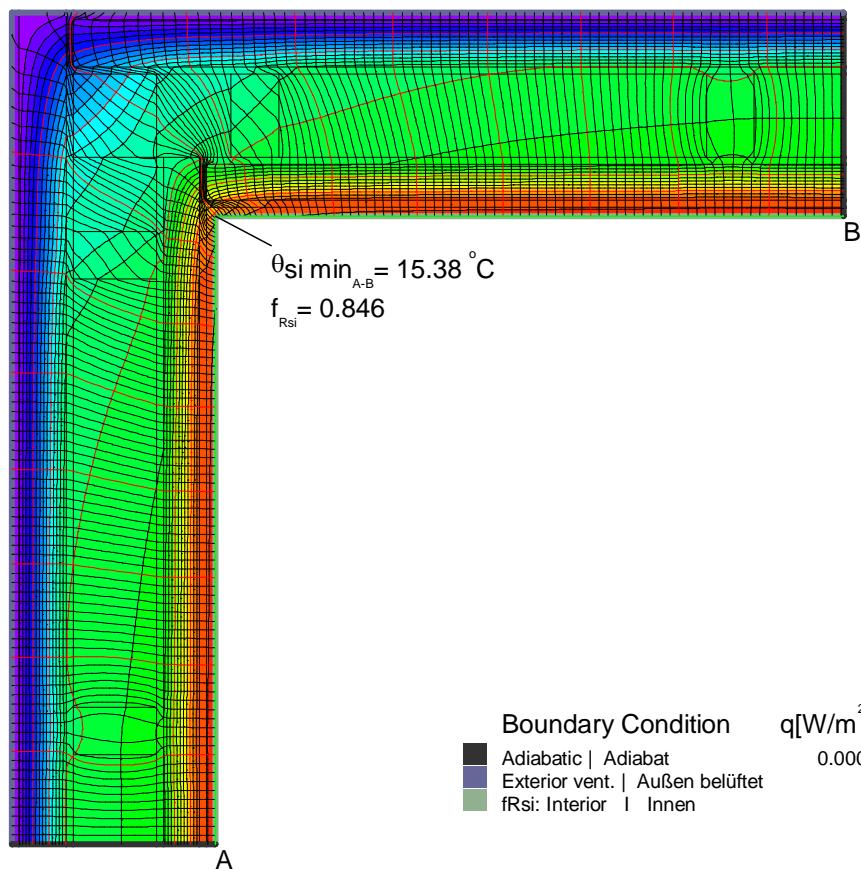
Airtightness concept

Airtightness of the system is achieved in the following way: windows and doors are installed with permanently elastic sealing materials and suitable airtight connection membranes and profiles. The airtight layer of the wall is the interior gypsum fibre board of the outer panel. In the roof and floor slab where only one sandwich panel is used, the air tight layer remains on the interior gypsum fibre board of the panel. Joints between panels and connections with other building elements are sealed with Soudal Soudatight SP airtight paint.



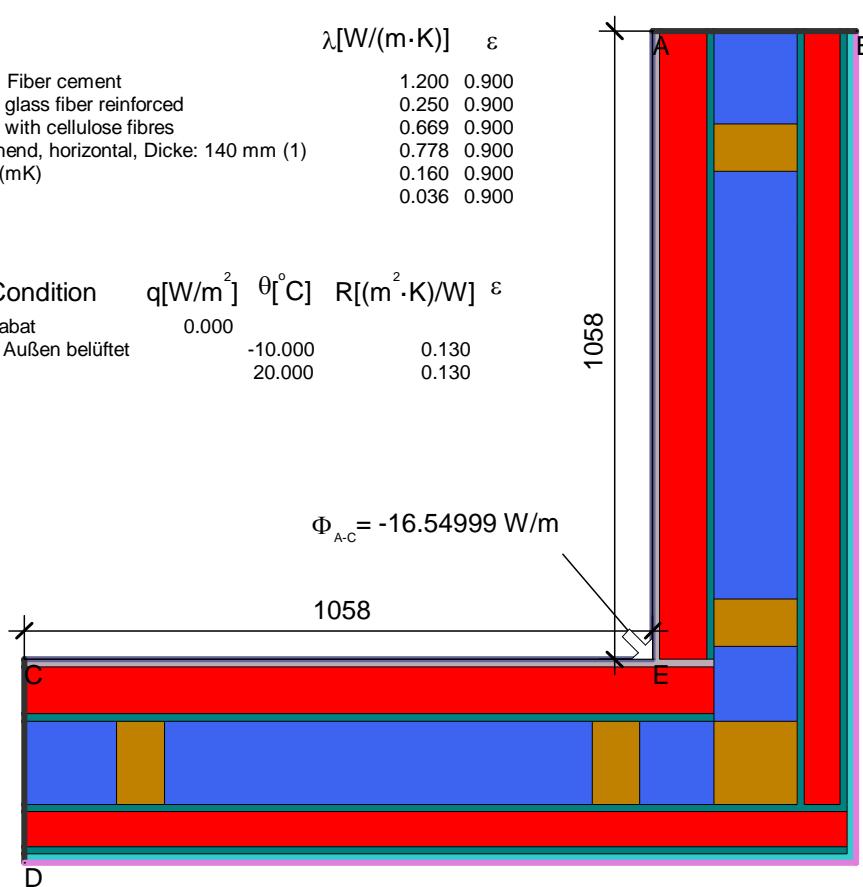


$$\psi_{A-E-C, \cdot} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{16.361}{30.000} - 0.224 \cdot 1.400 - 0.224 \cdot 1.400 = -0.081 \text{ W/(m}\cdot\text{K)}$$

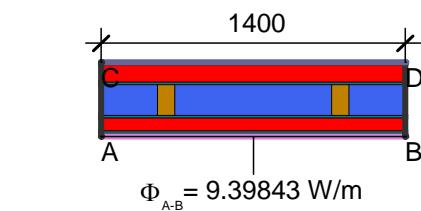


Material	$\lambda[W/(m \cdot K)]$	ε
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Luftschicht, ruhend, horizontal, Dicke: 140 mm (1)	0.778	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

Boundary Condition	$q[W/m^2]$	$\theta[^\circ C]$	$R[(m^2 \cdot K)/W]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet		-10.000	0.130	
Interior Innen		20.000	0.130	

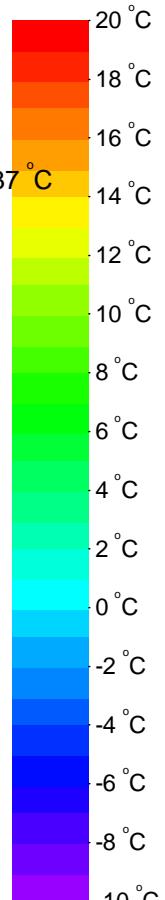
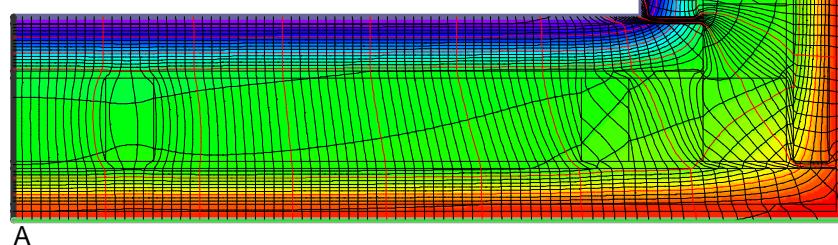


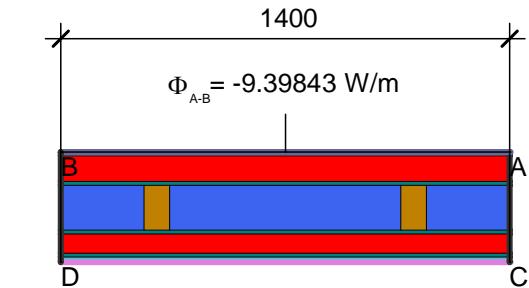
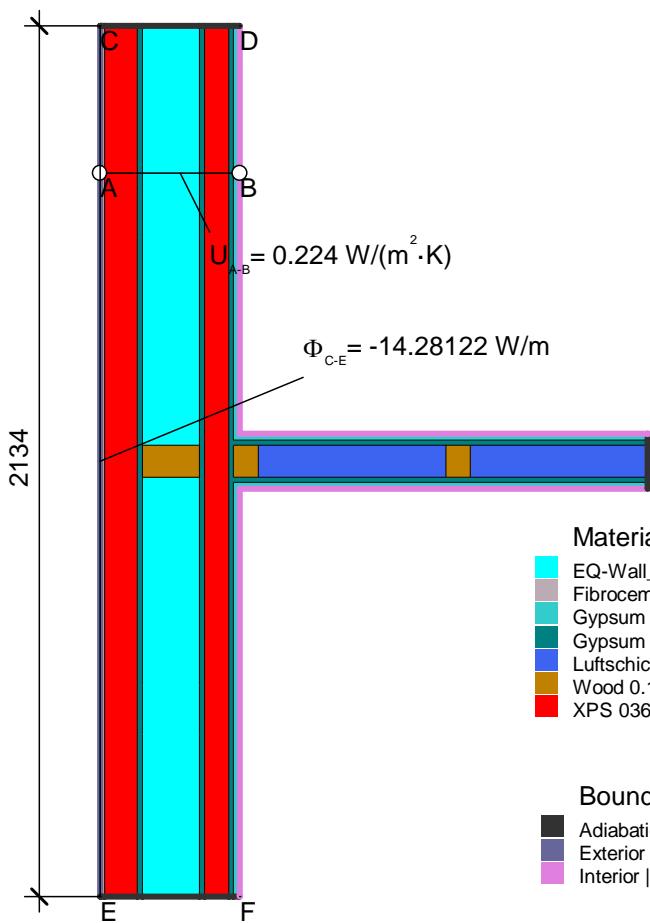
$$\psi_{A-E-C, \cdot} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{16.550}{30.000} - 0.224 \cdot 1.058 - 0.224 \cdot 1.058 = 0.078 \text{ W/(m} \cdot \text{K)}$$



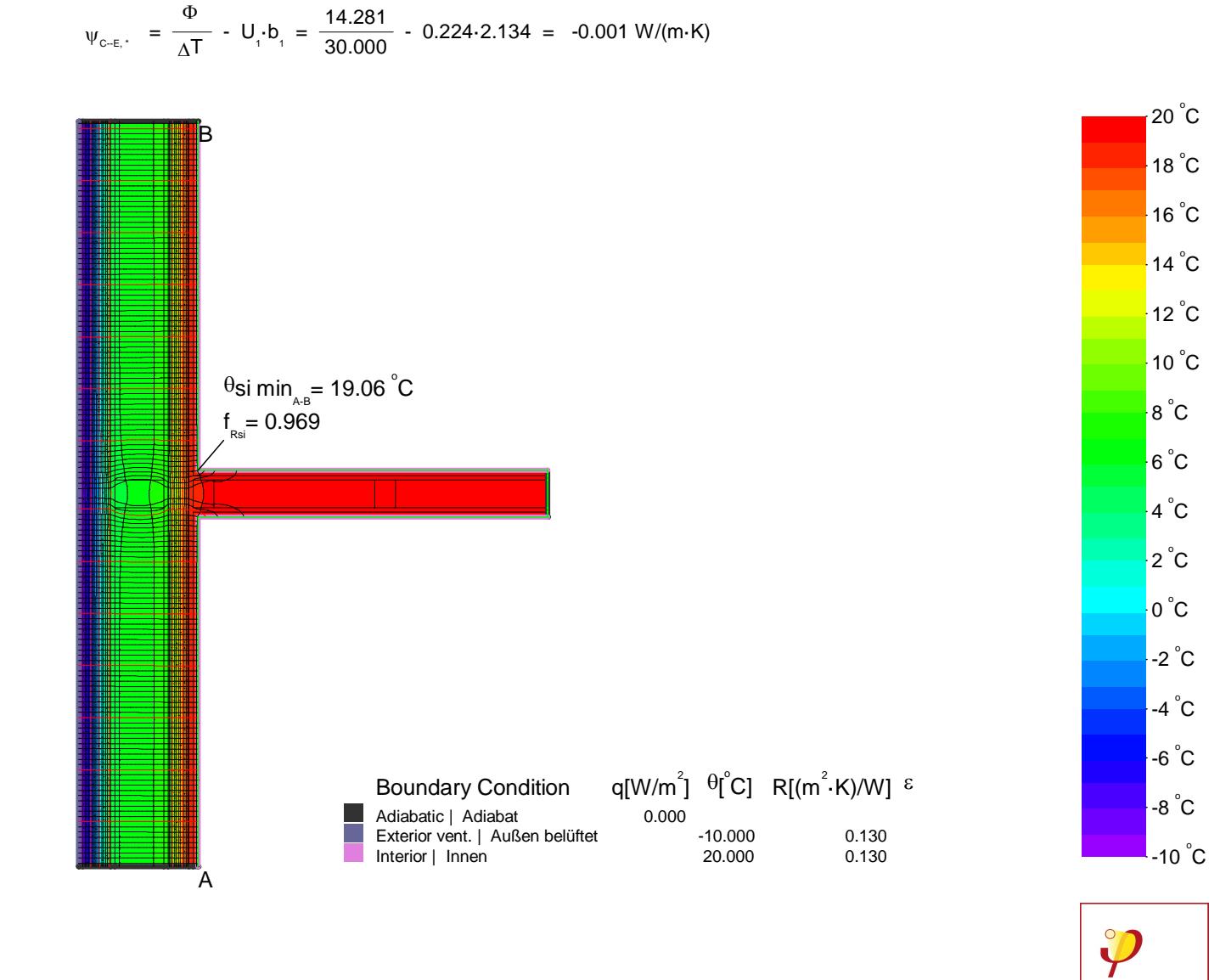
$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.398}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2 \cdot \text{K)}$$

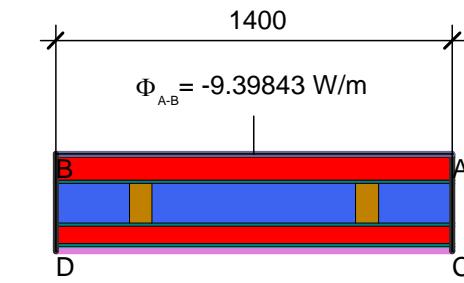
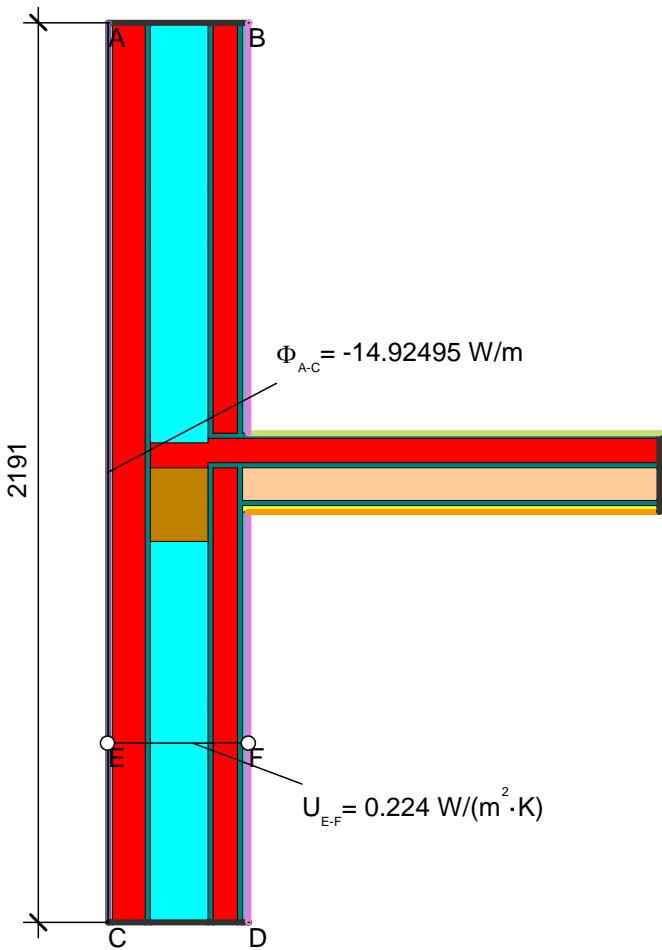
Boundary Condition	$q[W/m^2]$	$\theta[^\circ C]$	$R[(m^2 \cdot K)/W]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet		-10.000	0.130	
fRsi: Interior Innen		20.000	0.250	





$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.398}{30.000 \cdot 1.400} = 0.224 \text{ W}/(\text{m}^2 \cdot \text{K})$$





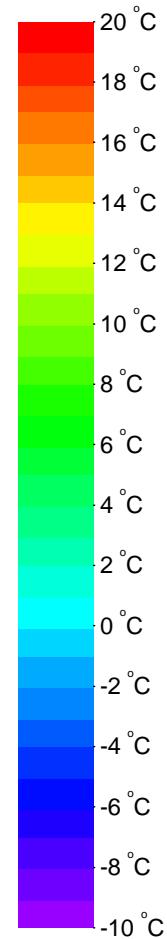
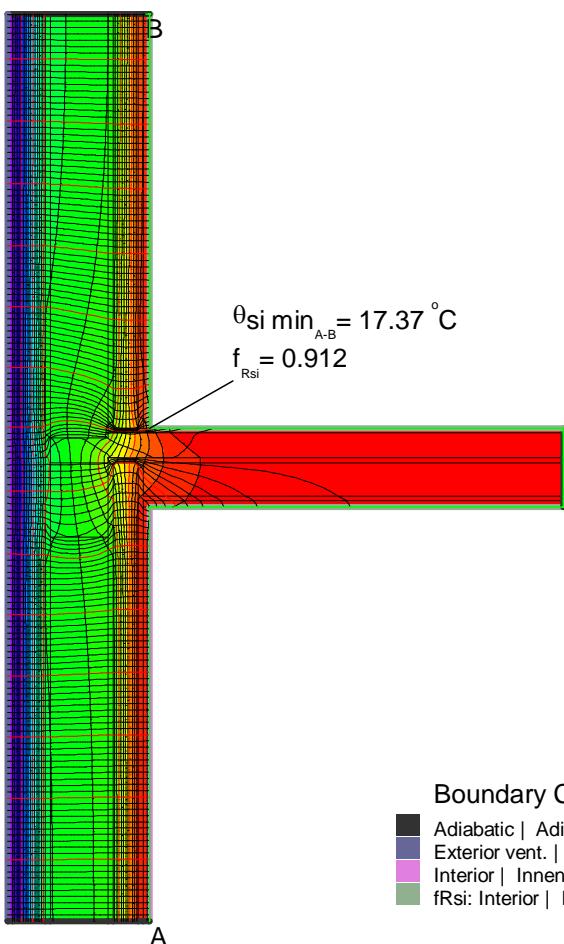
$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.398}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2\text{·K)}$$

Material

	$\lambda [\text{W}/(\text{m} \cdot \text{K})]$	ε
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board Gipskartonplatten 900 kg/m³ 10456	0.250	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Luftsicht, ruhend, aufwärts, Dicke: 80 mm	0.500	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

Boundary Condition	$q [\text{W}/\text{m}^2]$	$\theta [{}^\circ\text{C}]$	$R [(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000			0.130
Int. flux down Innen abwärts	20.000			0.170
Interior Innen	20.000			0.130
Interior up. Innen auf.	20.000			0.100
Interior Innen	20.000			0.130

$$\psi_{A-C,*} = \frac{\Phi}{\Delta T} \cdot U_1 \cdot b_1 = \frac{14.925}{30.000} \cdot 0.224 \cdot 2.191 = 0.007 \text{ W/(m·K)}$$



Boundary Condition	$q [\text{W}/\text{m}^2]$	$\theta [{}^\circ\text{C}]$	$R [(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000			0.130
Interior Innen	20.000			0.130





Certification report | Zertifizierungsbericht

Passive House Institute

Building system Bausystem

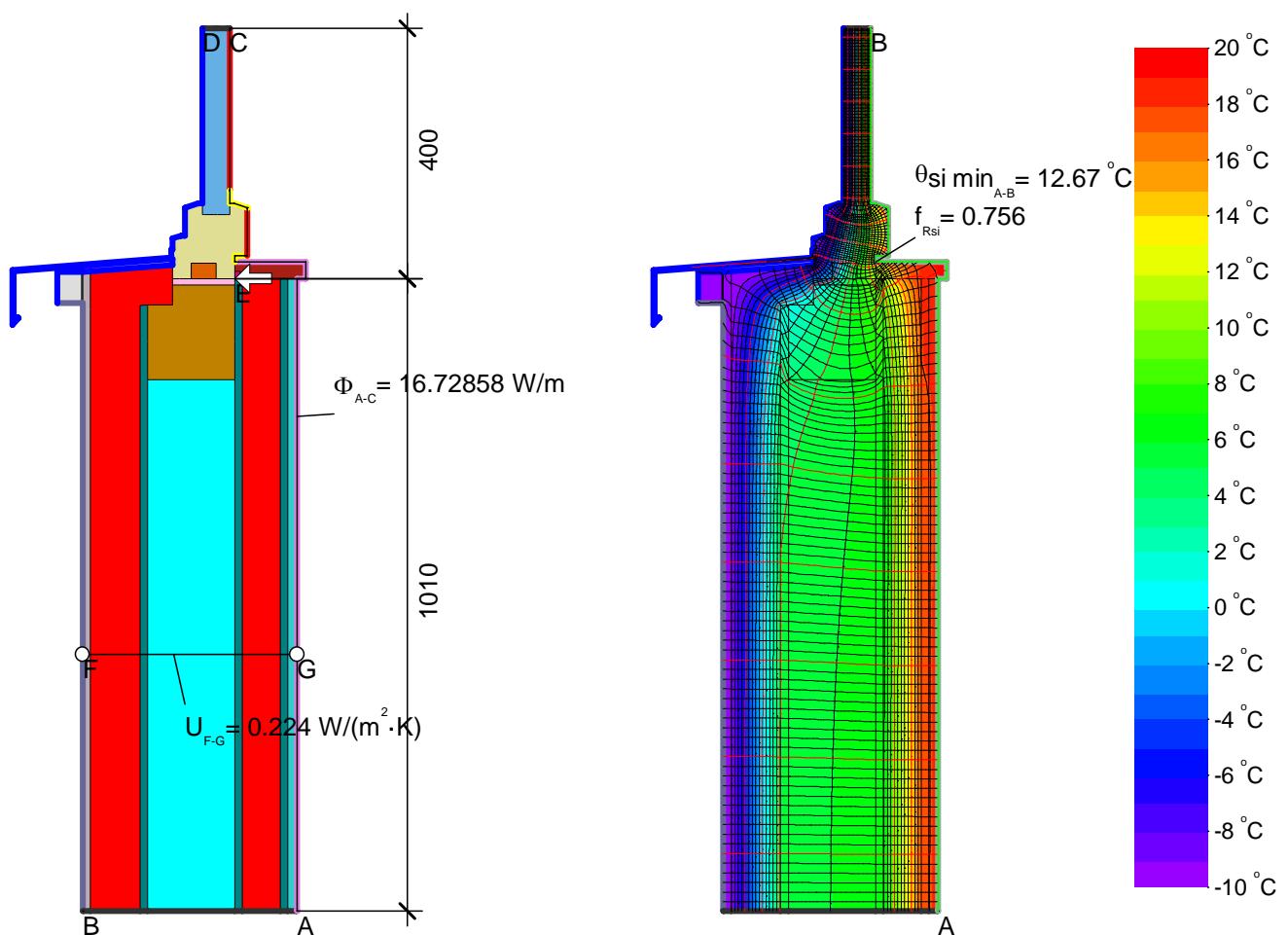


for the warm, temperate climate
für das warm-gemäßiges Klima

Product Produkt:	Thermochip HOUSING SATE-WALL
Client Auftraggeber:	Thermochip SLU
Instruction Konstruktion	Lightweight timber construction Holzleichtbau
Contact person Ansprechpartner Website	Diego Rodriguez +34 681 155 131 www.thermochip.com
Date Datum: Author Autor:	15.09.2020 M. Arch Soraya López García

+49.6151.82699.0
mail@passiv.de
www.passiv.de

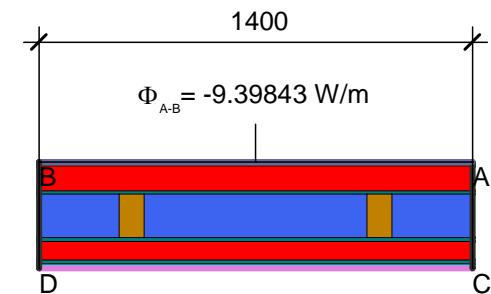
Passive House Institute
Rheinstraße 44/46
64283 Darmstadt
GERMANY



$$\psi_{A-E-C,\dots} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - \frac{\Phi_2}{\Delta T} = \frac{16.729}{30.000} - 0.224 \cdot 1.010 - \frac{9.453}{30.000} = 0.016 \text{ W/(m}\cdot\text{K)}$$

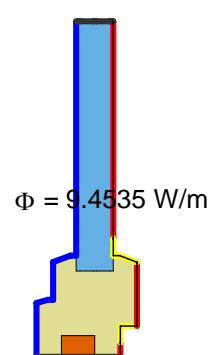
Material	$\lambda[\text{W}/(\text{m}\cdot\text{K})]$	ε
Aluminum Aluminium 10456	160.000	0.900
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Hardwood Hartholz 0.18 700 kg/m³ 10456	0.180	0.900
Insulation Wärmedämmung 050	0.050	0.900
PU in-situ foam PU-Ortschaum 040	0.040	0.900
Panel Maske	0.035	0.900
Silicone Silikon	0.350	0.900
Softwood, OSB Weichholz, OSB ISO 10456	0.130	0.900
Unvent. cavity unbel. Hohlr. *		
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

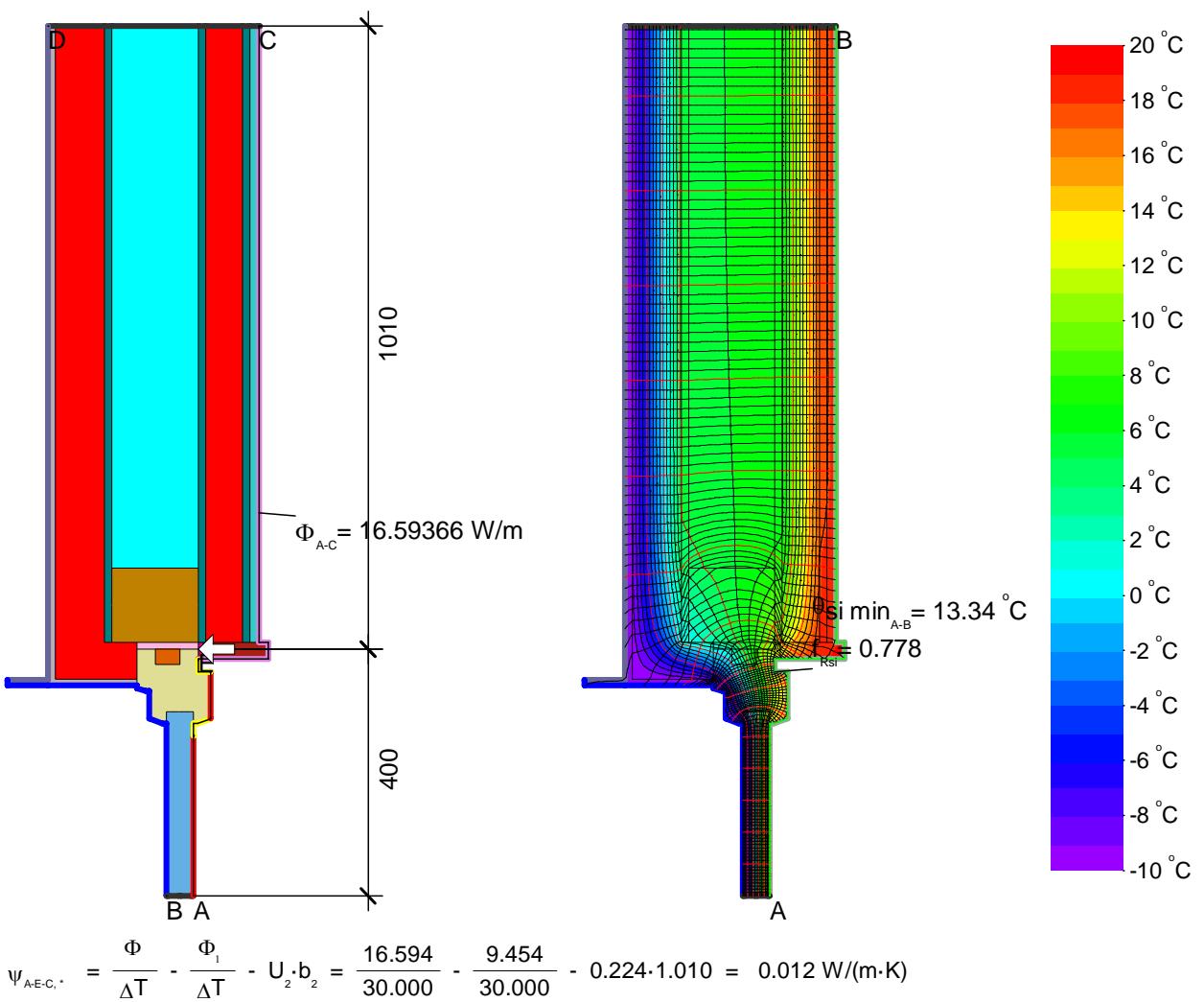
* EN ISO 10077-2:2017, 6.4.3



$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.398}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2\cdot\text{K)}$$

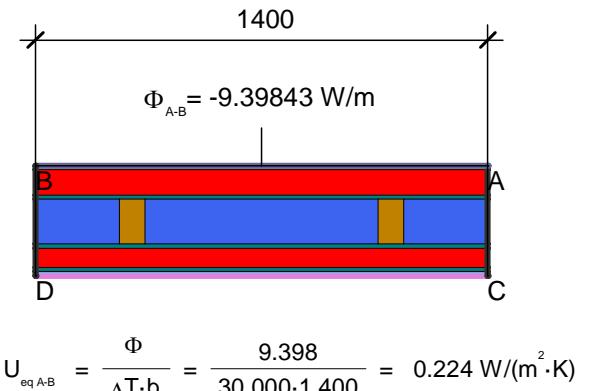
Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[{}^\circ\text{C}]$	$R[(\text{m}^2\cdot\text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000	0.130		
Exterior Außen	-10.000	0.040		
Innen Fensterrahmen Reduziert	20.000	0.200		
Innen Fensterrahmen Standard	20.000	0.130		
Interior Innen	20.000	0.130		
e 0,9 Cavity Hohlraum		0.900		





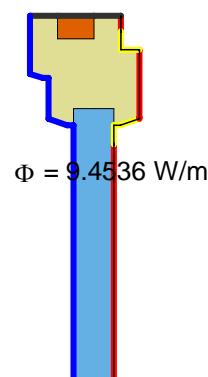
$$\Psi_{A-E-C, \cdot} = \frac{\Phi}{\Delta T} - \frac{\Phi_i}{\Delta T} - U_2 \cdot b_2 = \frac{16.594}{30.000} - \frac{9.454}{30.000} - 0.224 \cdot 1.010 = 0.012 \text{ W/(m}\cdot\text{K)}$$

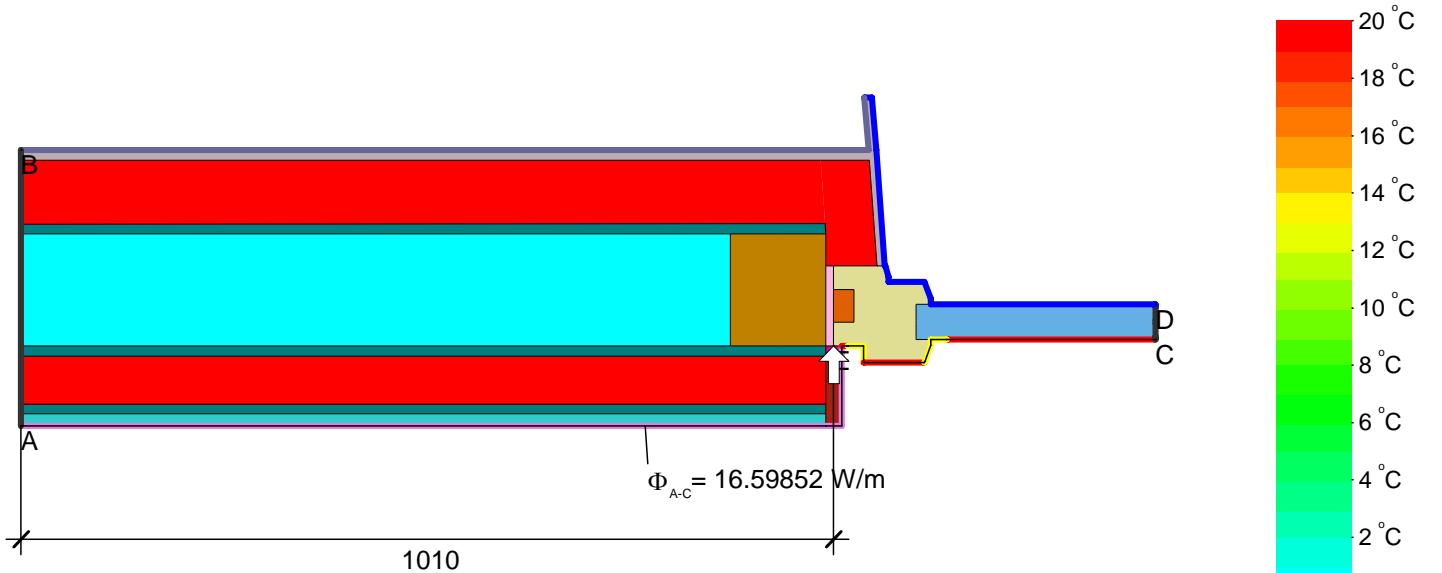
Material	$\lambda[\text{W}/(\text{m}\cdot\text{K})]$	ε
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Hardwood I Hartholz 0.18 700 kg/m³ 10456	0.180	0.900
Insulation I Wärmedämmung 050	0.050	0.900
PU in-situ foam I PU-Ortschaum 040	0.040	0.900
Panel I Maske	0.035	0.900
Silicone I Silikon	0.350	0.900
Softwood, OSB I Weichholz, OSB ISO 10456	0.130	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900



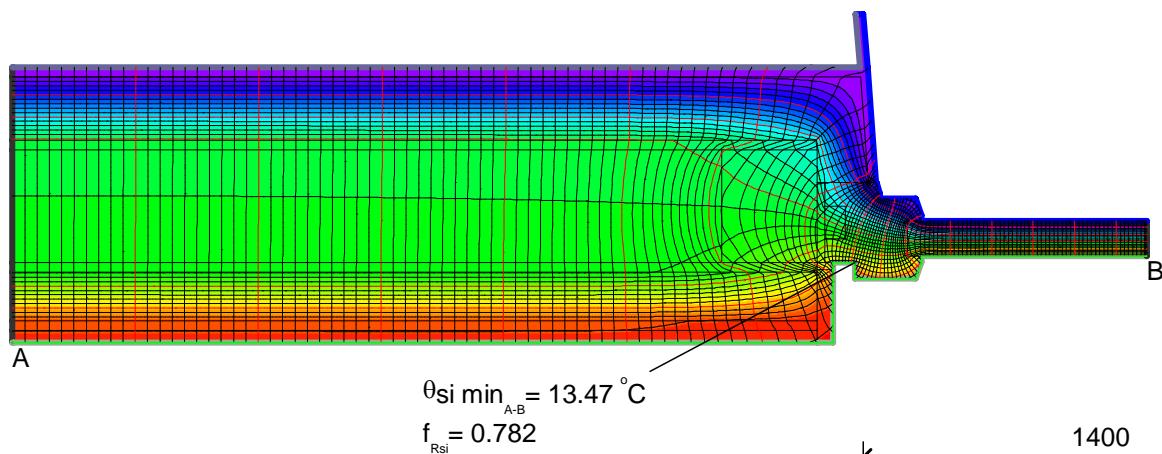
$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.398}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2 \cdot \text{K)}$$

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^\circ\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Aussen Standard		-10.000	0.040	
Exterior vent. Außen belüftet		-10.000	0.130	
Innen Fensterrahmen Reduziert		20.000	0.200	
Innen Fensterrahmen Standard		20.000	0.130	
Interior Innen		20.000	0.130	

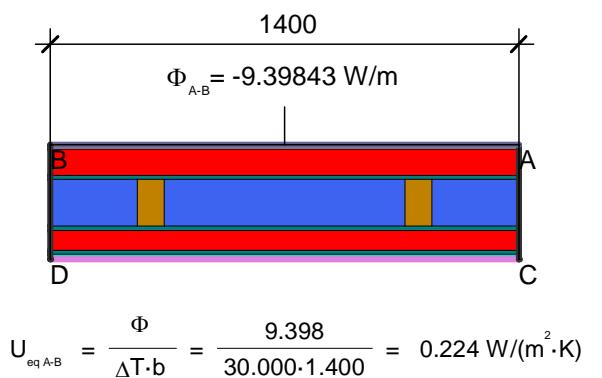




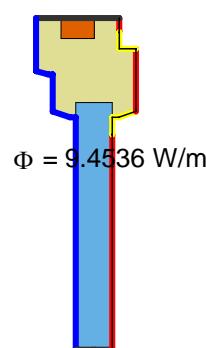
$$\psi_{A-E-C,*} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - \frac{\Phi_2}{\Delta T} = \frac{16.599}{30.000} - 0.224 \cdot 1.010 - \frac{9.454}{30.000} = 0.012 \text{ W/(m·K)}$$



Material	$\lambda[\text{W}/(\text{m} \cdot \text{K})]$	ϵ
EQ-Wall_Air layer + timber	0.666	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Hardwood Hartholz 0.18 700 kg/m³ 10456	0.180	0.900
Insulation Wärmemedämmung 050	0.050	0.900
PU in-situ foam PU-Ortschaum 040	0.040	0.900
Panel Maske	0.035	0.900
Silicone Silikon	0.350	0.900
Softwood, OSB Weichholz, OSB ISO 10456	0.130	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

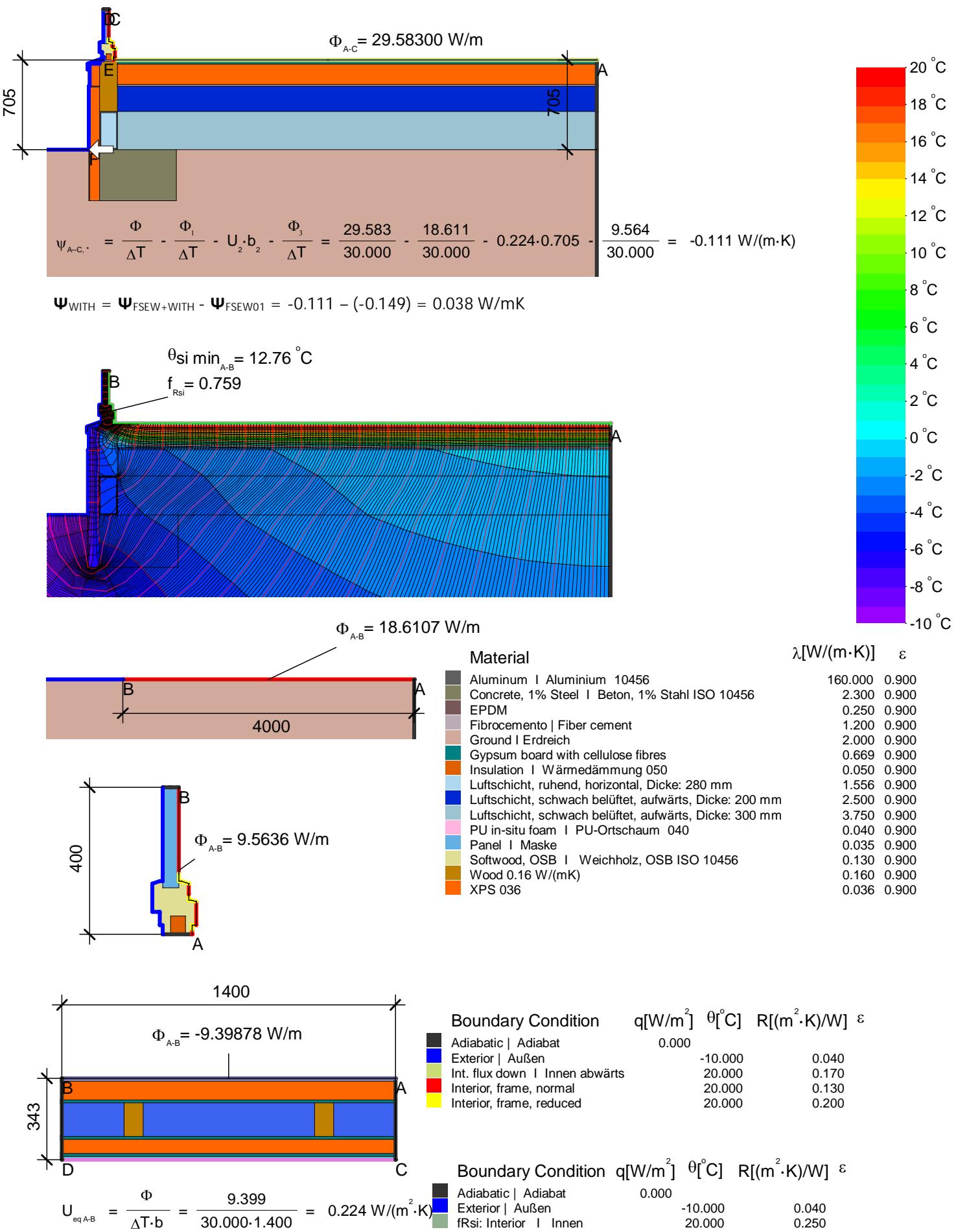


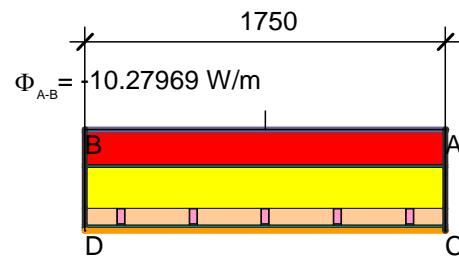
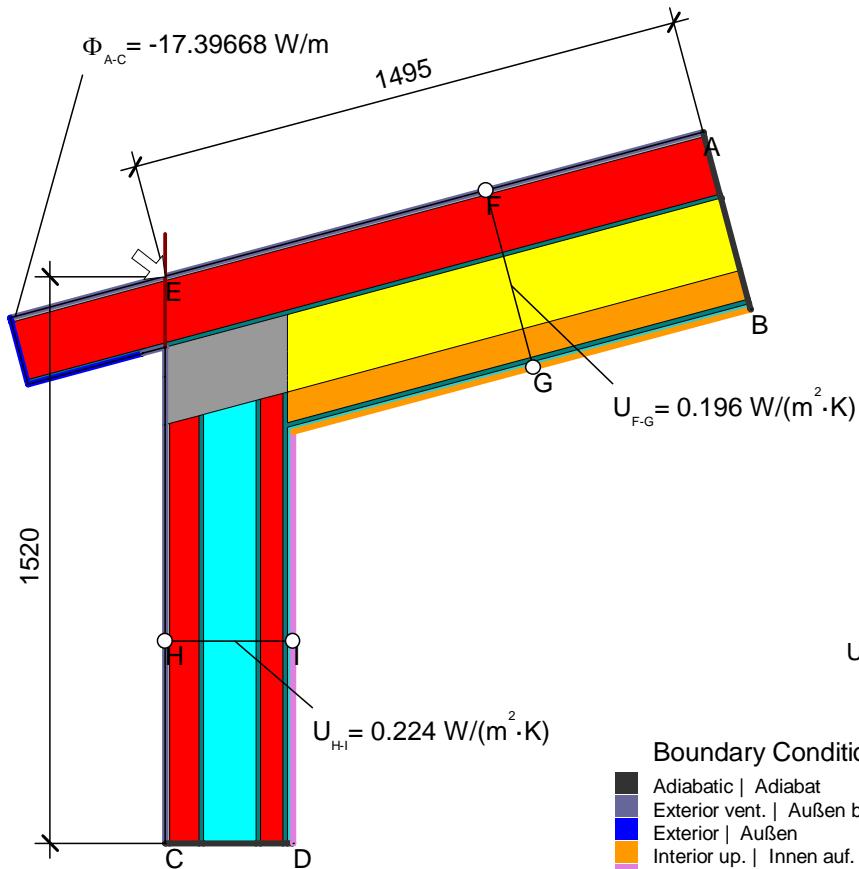
$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.398}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2 \cdot \text{K)}$$



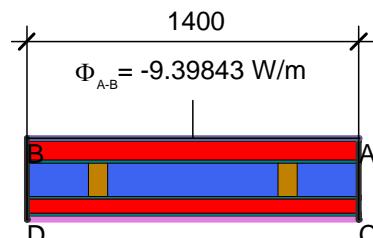
Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[{}^{\circ}\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ϵ
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet		-10.000	0.130	
Exterior Außen		-10.000	0.040	
Innen Fensterrahmen Reduziert		20.000	0.200	
Innen Fensterrahmen Standard		20.000	0.130	
Interior Innen		20.000	0.130	







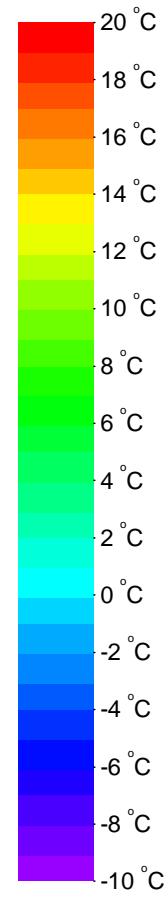
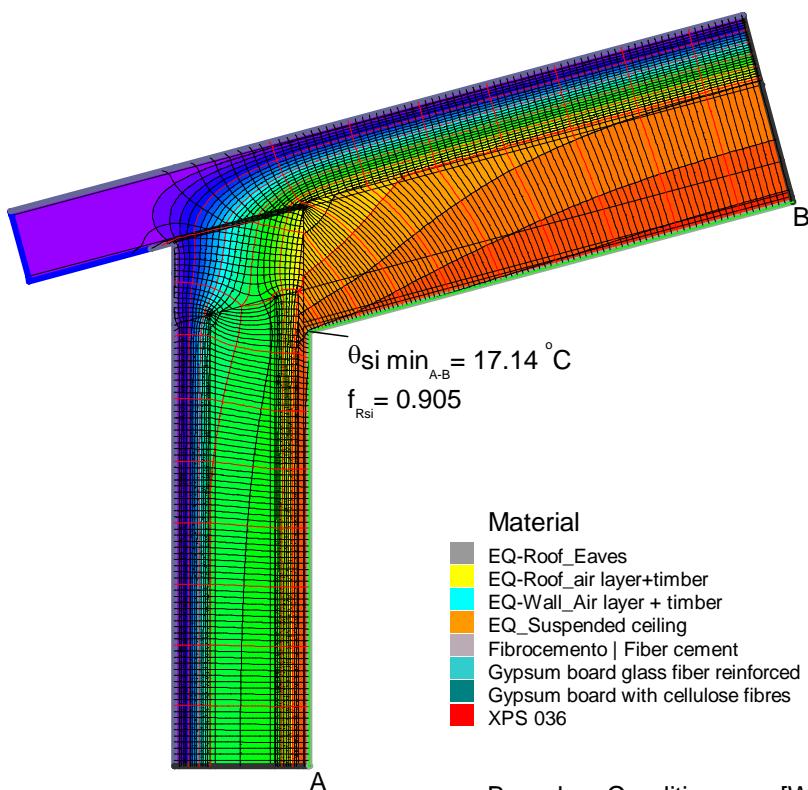
$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{10.280}{30.000 \cdot 1.750} = 0.196 \text{ W/(m}^2\text{K)}$$



$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.398}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2\text{K)}$$

Boundary Condition	$q[\text{W/m}^2]$	$\theta[^\circ\text{C}]$	$R[(\text{m}^2\text{-K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000		0.130	
Exterior Außen	-10.000		0.040	
Interior up. Innen auf.	20.000		0.100	
Interior Innen	20.000		0.130	

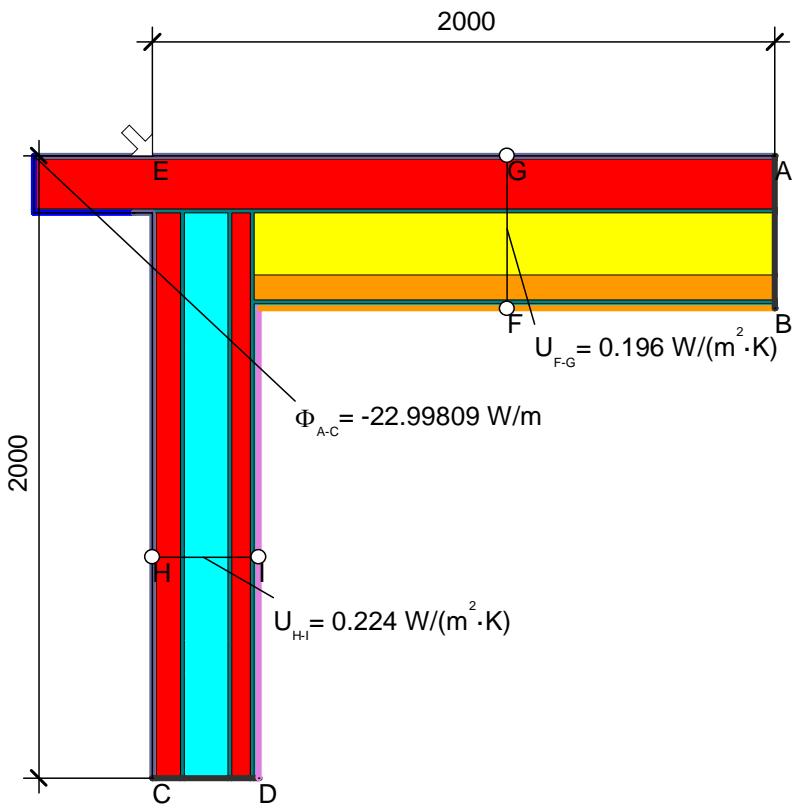
$$\psi_{A-E-C, \cdot} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{17.397}{30.000} - 0.196 \cdot 1.495 - 0.224 \cdot 1.520 = -0.053 \text{ W/(m}\cdot\text{K)}$$



Material	$\lambda[\text{W}/(\text{m}\cdot\text{K})]$	ε
EQ-Roof_Eaves	0.080	0.900
EQ-Roof_air layer+timber	0.920	0.900
EQ-Wall_Air layer + timber	0.666	0.900
EQ_Suspended ceiling	0.710	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
XPS 036	0.036	0.900

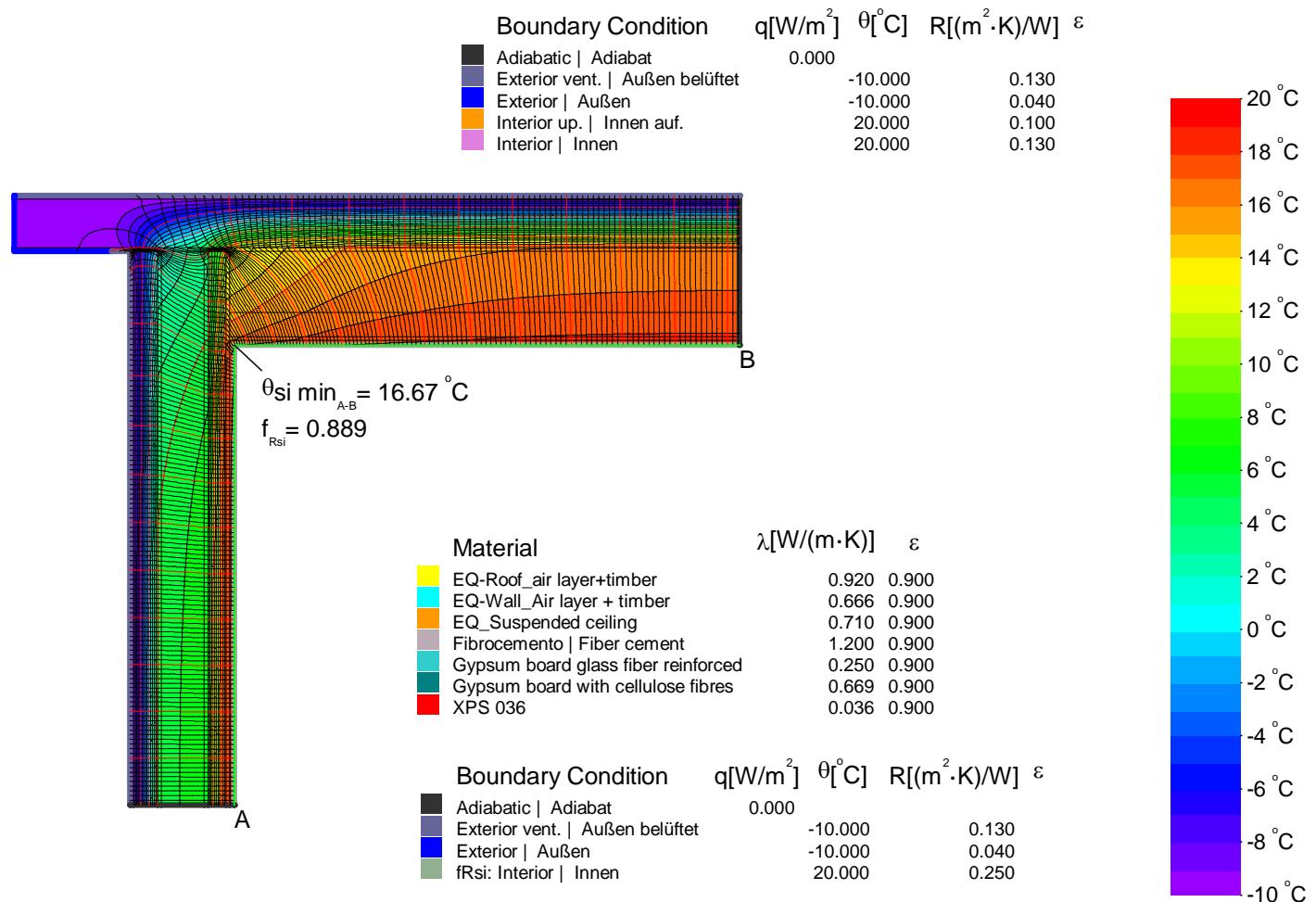
Boundary Condition	$q[\text{W/m}^2]$	$\theta[^\circ\text{C}]$	$R[(\text{m}^2\text{-K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000		0.130	
Exterior Außen	-10.000		0.040	
fRsi: Interior Innen	20.000		0.250	

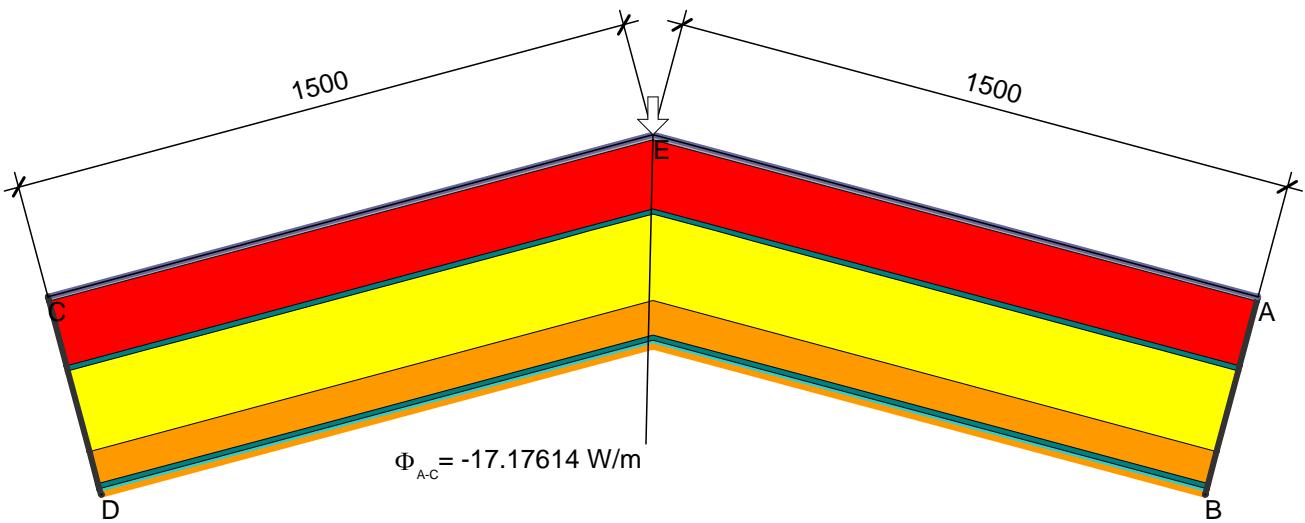




$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{10.280}{30.000 \cdot 1.750} = 0.196 \text{ W}/(\text{m}^2 \cdot \text{K})$$

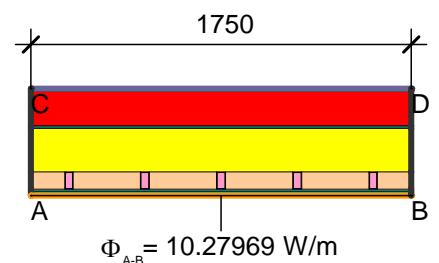
$$\psi_{A-E-C,-} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{22.998}{30.000} - 0.196 \cdot 2.000 - 0.224 \cdot 2.000 = -0.073 \text{ W}/(\text{m} \cdot \text{K})$$





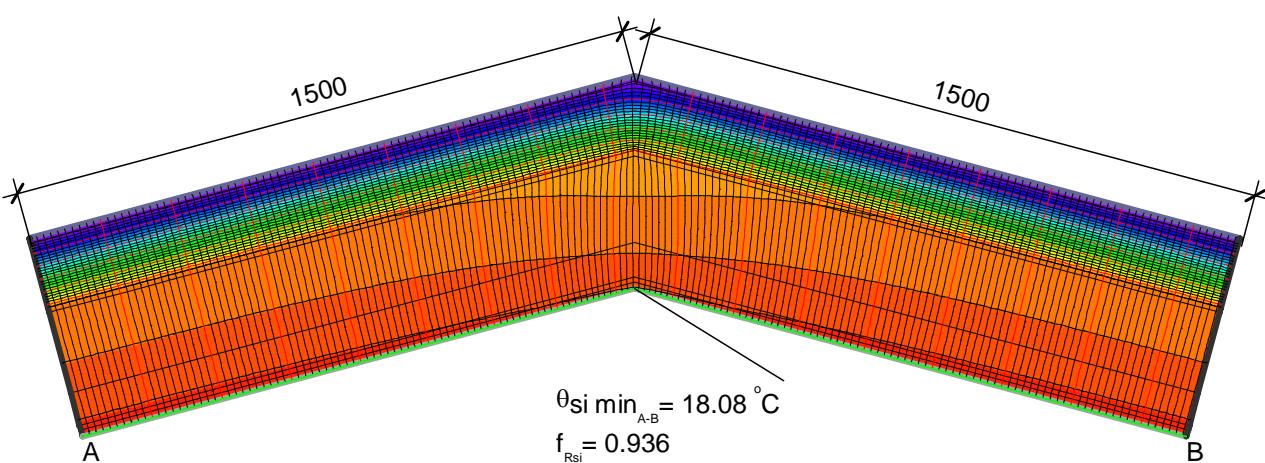
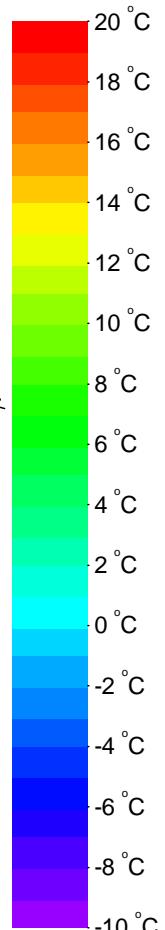
$$\psi_{A-E-C,-} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{17.176}{30.000} - 0.196 \cdot 1.500 - 0.196 \cdot 1.500 = -0.015 \text{ W/(m}\cdot\text{K)}$$

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^{\circ}\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000	-10.000	0.130	
Exterior vent. Außen belüftet		20.000		
Interior up. Innen auf.			0.100	



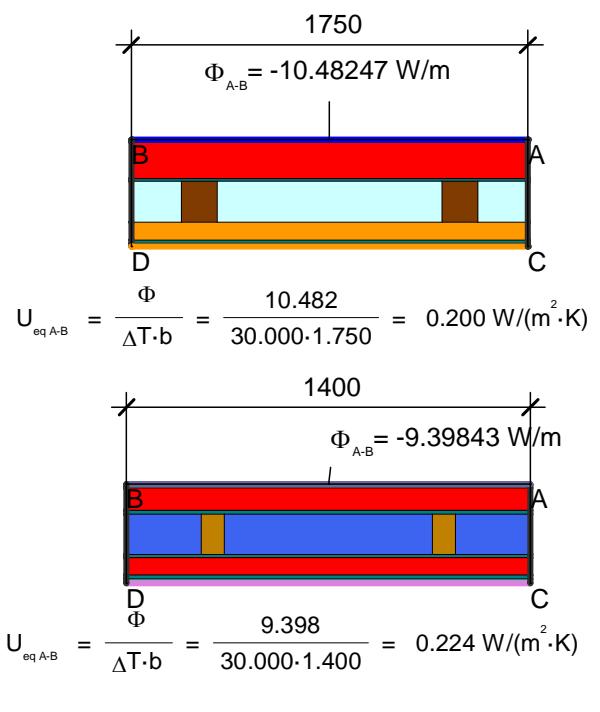
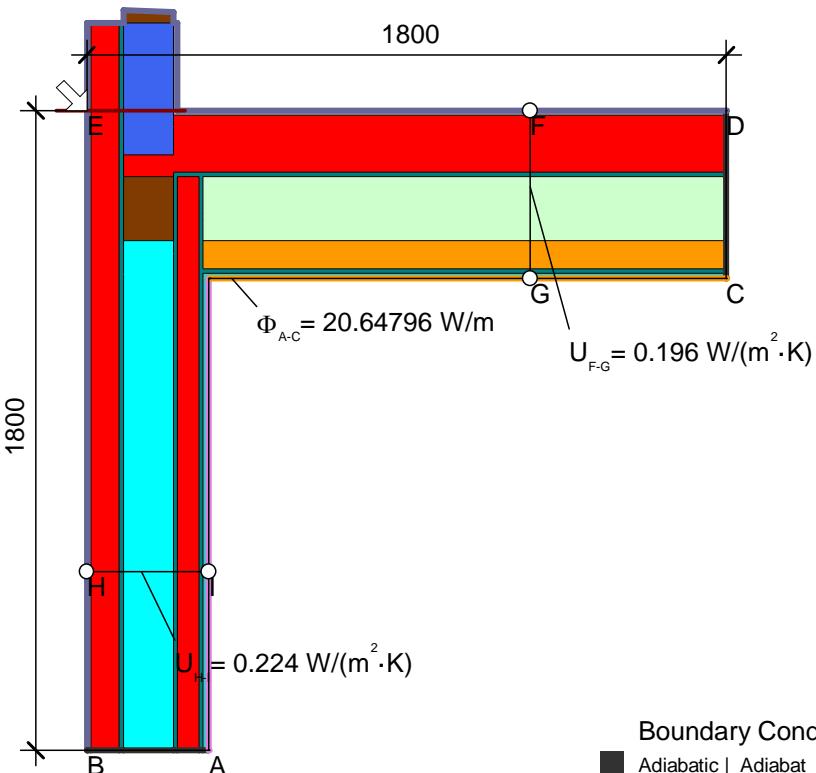
Material	$\lambda[\text{W}/(\text{m}\cdot\text{K})]$	ε
EQ-Roof_air layer+timber	0.920	0.900
EQ_Suspended ceiling	0.710	0.900
Fibrocemento Fiber cement	1.200	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
XPS 036	0.036	0.900

$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{10.280}{30.000 \cdot 1.750} = 0.196 \text{ W}/(\text{m}^2 \cdot \text{K})$$



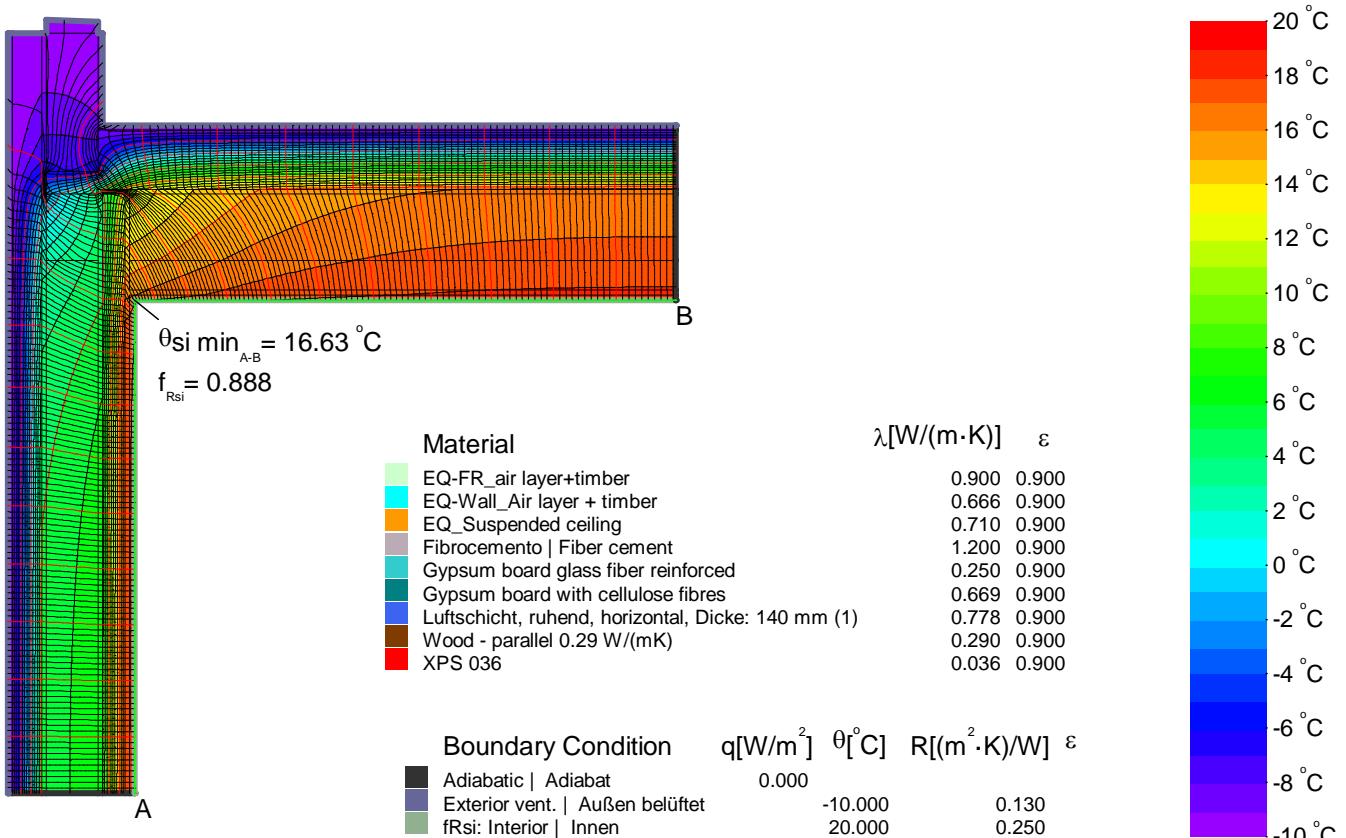
Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta[^{\circ}\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000	-10.000	0.130	
Exterior vent. Außen belüftet		20.000		

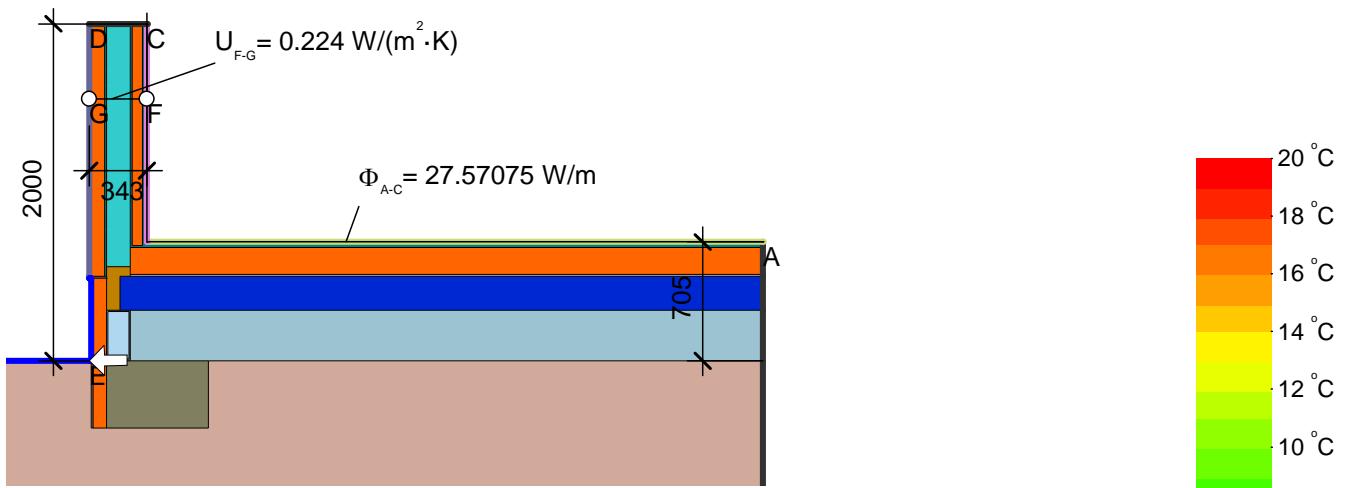




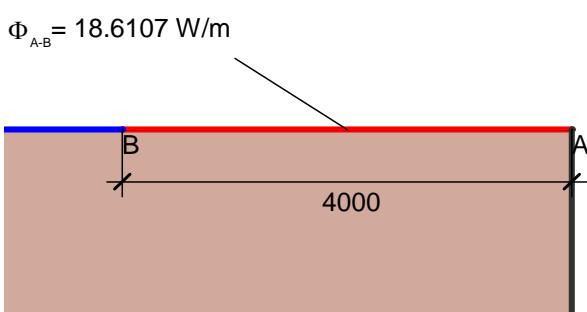
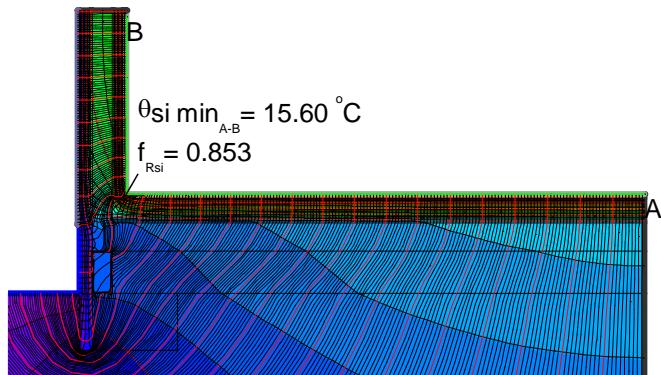
Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta [{}^\circ \text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic Adiabat	0.000			
Exterior vent. Außen belüftet	-10.000		0.130	
Interior Innen	20.000		0.130	
Interior up. Innen auf.	20.000		0.100	

$$\psi_{A-E-C,-} = \frac{\Phi}{\Delta T} - U_1 \cdot b_1 - U_2 \cdot b_2 = \frac{20.648}{30.000} - 0.224 \cdot 1.800 - 0.200 \cdot 1.800 = -0.074 \text{ W}/(\text{m} \cdot \text{K})$$

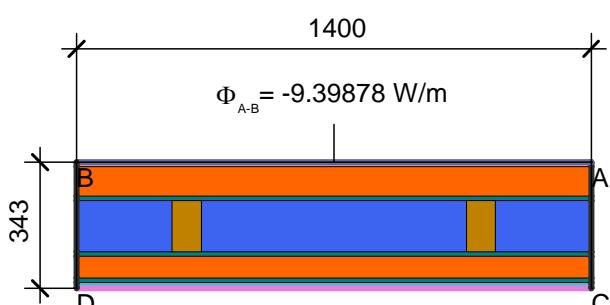




$$\psi_{A-E-C,+} = \frac{\Phi}{\Delta T} - \frac{\Phi_1}{\Delta T} - U_2 \cdot b_2 = \frac{27.571}{30.000} - \frac{18.611}{30.000} - 0.224 \cdot 2.000 = -0.149 \text{ W/(m·K)}$$



Material	$\lambda [\text{W}/(\text{m} \cdot \text{K})]$	ε
Aluminum Aluminium 10456	160.000	0.900
Concrete, 1% Steel Beton, 1% Stahl ISO 10456	2.300	0.900
EPDM	0.250	0.900
EQ-Wall_Air layer + timber	0.656	0.900
Fibrocemento Fiber cement	1.200	0.900
Ground Erdreich	2.000	0.900
Gypsum board glass fiber reinforced	0.250	0.900
Gypsum board with cellulose fibres	0.669	0.900
Luftschicht, ruhend, horizontal, Dicke: 280 mm	1.556	0.900
Luftschicht, schwach belüftet, aufwärts, Dicke: 200 mm	2.500	0.900
Luftschicht, schwach belüftet, aufwärts, Dicke: 300 mm	3.750	0.900
Wood 0.16 W/(mK)	0.160	0.900
XPS 036	0.036	0.900

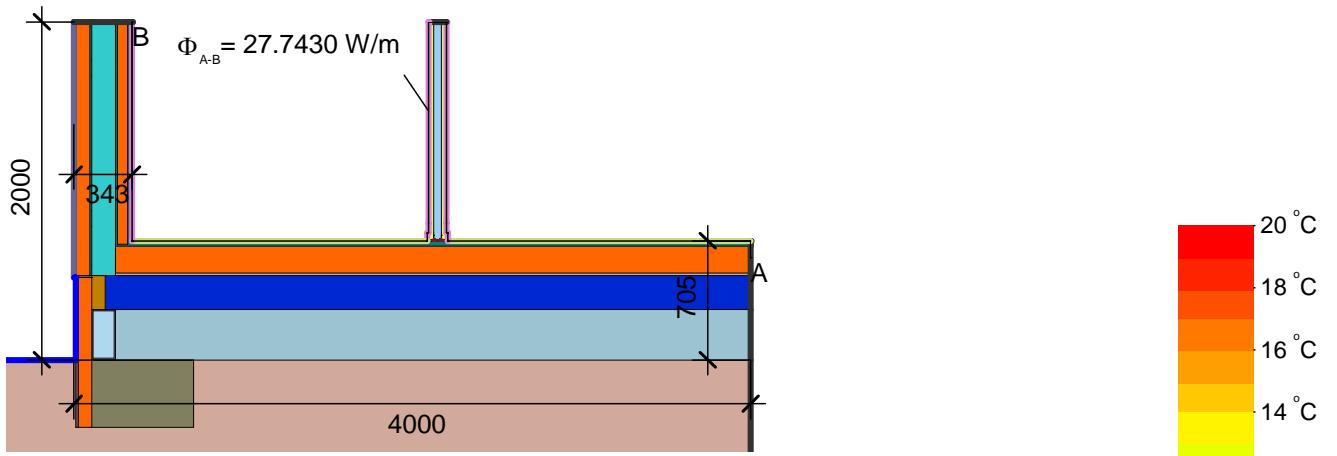


$$U_{eq A-B} = \frac{\Phi}{\Delta T \cdot b} = \frac{9.399}{30.000 \cdot 1.400} = 0.224 \text{ W/(m}^2 \cdot \text{K)}$$

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta [{}^{\circ}\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic	0.000			
Adiabatic Adiabat	0.000			
Exterior Außen		-10.000	0.040	
Exterior vent. Außen belüftet		-10.000	0.130	
Int. flux down Innen abwärts		20.000	0.170	
Interior Innen		20.000	0.130	

Boundary Condition	$q[\text{W}/\text{m}^2]$	$\theta [{}^{\circ}\text{C}]$	$R[(\text{m}^2 \cdot \text{K})/\text{W}]$	ε
Adiabatic	0.000			
Adiabatic Adiabat	0.000			
Exterior Außen		-10.000	0.040	
Exterior vent. Außen belüftet		-10.000	0.130	
fRsi: Interior Innen		20.000	0.250	





$$\Psi_{FSIW} = (Q_{FSIW} - Q_{FSEW}) / \Delta T = (27.7430 - 27.5708) / 30 = 0,006 \text{ W/mK}$$

